

13.42 HW #7 SOL'NS

1a. $\omega_n = \sqrt{\frac{k}{M + m_e}} = \sqrt{\frac{k}{M + \rho \pi d^2}}$

b. • FIRST, FIND :

$Re = \frac{Ud}{\nu} = \frac{(10)(0.1)}{10^{-6}} = 10^6$

• FROM "STROUHAL NUMBER vs. REYNOLDS NUMBER" IN READING 10, THE CORRESPONDING STROUHAL # FOR A SMOOTH CYLINDER IS:

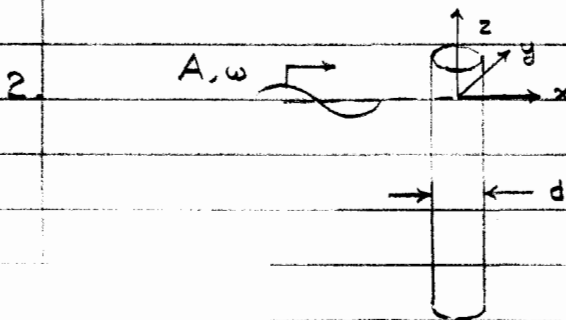
$St \approx 0.43$

• $St = \frac{f_v d}{U} \implies f_v = \frac{St \cdot U}{d} = \frac{0.43(10)}{0.1} = 43 \text{ s}^{-1}$

c. • $f_v \sim f_n = \frac{\omega_n}{2\pi} = \frac{1}{2\pi} \sqrt{\frac{k}{M + \rho \pi d^2}}$

• $f_c \sim f_n$ "

• $f_{DRAG} \sim 2f_n$



• $\zeta(x, t) = A \text{Re} \{ e^{-ikx + i\omega t} \}$

• $\phi(x, z, t) = \text{Re} \left\{ \frac{i g A}{\omega} e^{kz - ikx + i\omega t} \right\}$

e. GIVEN $\lambda \gg d \in A \sim 2d$, or $\frac{h}{d} \sim 4 \implies$ USE MORISON EQ.:

$dF_x(x=0, z, t) = \left(e^{\frac{\pi d^2}{4}} + m_a \right) \frac{\partial u}{\partial t} dz + \frac{1}{2} \rho C_D du |u| dz$

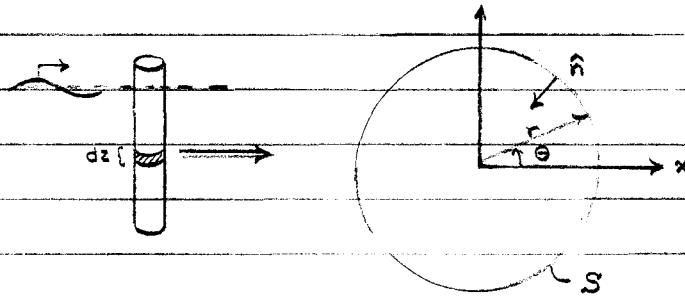
WHERE $m_0 = \rho \frac{\pi d^2}{4}$ AND $u = \frac{\partial \phi}{\partial x}$.

b. THE FROUDE-KRYLOV TERM FROM a IS

$$\rho \frac{\pi d^2}{4} \frac{\partial u}{\partial t} dz \Big|_{x=0} \quad (1)$$

HORIZONTAL FORCE DUE TO UNSTEADY PRESSURE INDUCED BY THE UNDISTURBED AMBIENT WAVES IS AS FOLLOWS:

- $p = -\rho \frac{\partial \phi}{\partial t} = \text{Re} \{ \rho g A e^{kz - ikx + i\omega t} \}$



- $$dF_x = \iint_S p \hat{n} \cdot \hat{i} ds$$

$$= \int_0^{2\pi} \text{Re} \{ \rho g A e^{kz} e^{-ikr \cos \theta + i\omega t} \} (-\cos \theta) dz r d\theta \Big|_{r=d/2}$$

$$= -\rho g A e^{kz} \frac{d}{2} dz \int_0^{2\pi} \cos(\omega t - k \frac{d}{2} \cos \theta) \cos \theta d\theta$$

$$= -\rho g A e^{kz} \frac{d}{2} dz \int_0^{2\pi} \left[\cos \omega t \cdot \cos \left(\frac{kd}{2} \cos \theta \right) + \right.$$

$$\left. + \sin \omega t \sin \left(\frac{kd}{2} \cos \theta \right) \right] \cos \theta d\theta$$

- IF $\lambda \gg d$, THEN $kd \ll 1$ AND $\cos \left(\frac{kd}{2} \cos \theta \right) \rightarrow 1$
 $\sin \left(\frac{kd}{2} \cos \theta \right) \rightarrow \frac{kd}{2} \cos \theta$

• THEN

$$dF_x \approx -\rho g A e^{kz} \frac{d}{2} dz \int_0^{2\pi} (\cos \omega t \cos \theta - \sin \omega t \frac{\pi d}{2} \cos^2 \theta) d\theta$$

$$= -\rho g A e^{kz} \frac{d}{2} dz \cdot \left(\frac{k d}{2} \pi \sin \omega t \right)$$

• NOTE THAT

$$\left. \frac{\partial u}{\partial t} \right|_{x=0} = \frac{\partial^2 \phi}{\partial x \partial t} = -A \omega^2 e^{kz} \sin \omega t \stackrel{\text{DISP. REL.}}{\downarrow} = -A g k e^{kz} \sin \omega t$$

$$\therefore dF_x \approx \rho \frac{\pi d^2}{4} \left. \frac{\partial u}{\partial t} \right|_{x=0} dz \quad \checkmark$$

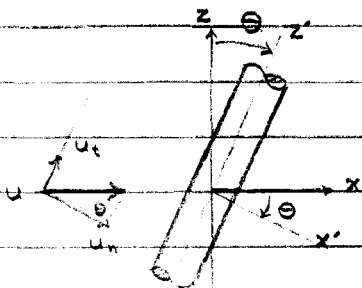
c. THE ADDED MASS TERM REPRESENTS THE DIFFRACTION FORCE.

d. THE PRESENCE OF A STRUCTURE WITH DIAMETER $\sim O(\lambda)$ WILL SIGNIFICANTLY DISTURB THE AMBIENT WAVE FIELD.

DEEP WATER: $\phi = \text{Re} \left\{ \frac{\rho g A}{\omega} e^{kz - ikx + i\omega t} \right\}$

$$u = \frac{\partial \phi}{\partial x} = \text{Re} \left\{ \omega A e^{kz - ikx + i\omega t} \right\}$$

SEPARATION PRINCIPLE (NEGLECTING VERTICAL VELOCITIES)



$$\theta = 15^\circ$$

$$u_n = u \cos \theta$$

$$u_t = u \sin \theta$$

$$\bullet dF_n = (\rho \nabla + m_a) \frac{\partial u_p}{\partial t} dz' + \frac{1}{2} \rho C_D d |u_n| u_n dz'$$

$$\bullet dF_t = \frac{1}{2} \rho C_F (\pi d) u_t |u_t| dz'$$

$$dz' = dz \cos \theta$$

$$\text{LIFT: } dF_L = -dF_n \sin \theta + dF_t \cos \theta$$

$$\text{DRAG: } dF_D = dF_n \cos \theta + dF_t \sin \theta$$

b. FOR A VERTICAL CYLINDER, THE DRAG FORCE WILL BE ENTIRELY DUE TO THE NORMAL COMPONENT.

$$\text{- i.e., } dF_D = dF_n = (\rho \nabla + m_a) \frac{\partial u}{\partial t} dz + \frac{1}{2} \rho C_D d |u| u dz$$

4a. $|F_x| \sim |F_z| = 5.6 \times 10^4 \text{ N.}$

b. $F_x(t) = F_I(t) + F_V(t)$
INERTIA, VISCIOUS DRAG TERM

$$\bullet |F_x| \gg |F_y|$$

• SINCE $F_x \sim \frac{\partial u}{\partial t}$, WHICH IS 90° OUT-OF-PHASE WITH $\gamma(t)$, THE MAXIMA OCCUR WHEN $\gamma = 0$.

d. $M_{\text{SEAFLOOR}} = \int_{-H}^0 (H+z) dF_x$ WHERE

$$dF_x = (\rho \nabla + m_a) \frac{\partial u}{\partial t} dz + \frac{1}{2} \rho C_D d |u| u dz$$

$$e. \quad z_{cp} = \frac{\int_{-H}^0 z \, dF_x}{\int_{-H}^0 dF_x}$$

RELATIVE TO THE SEAFLOOR, $H + z_{cp}$.