

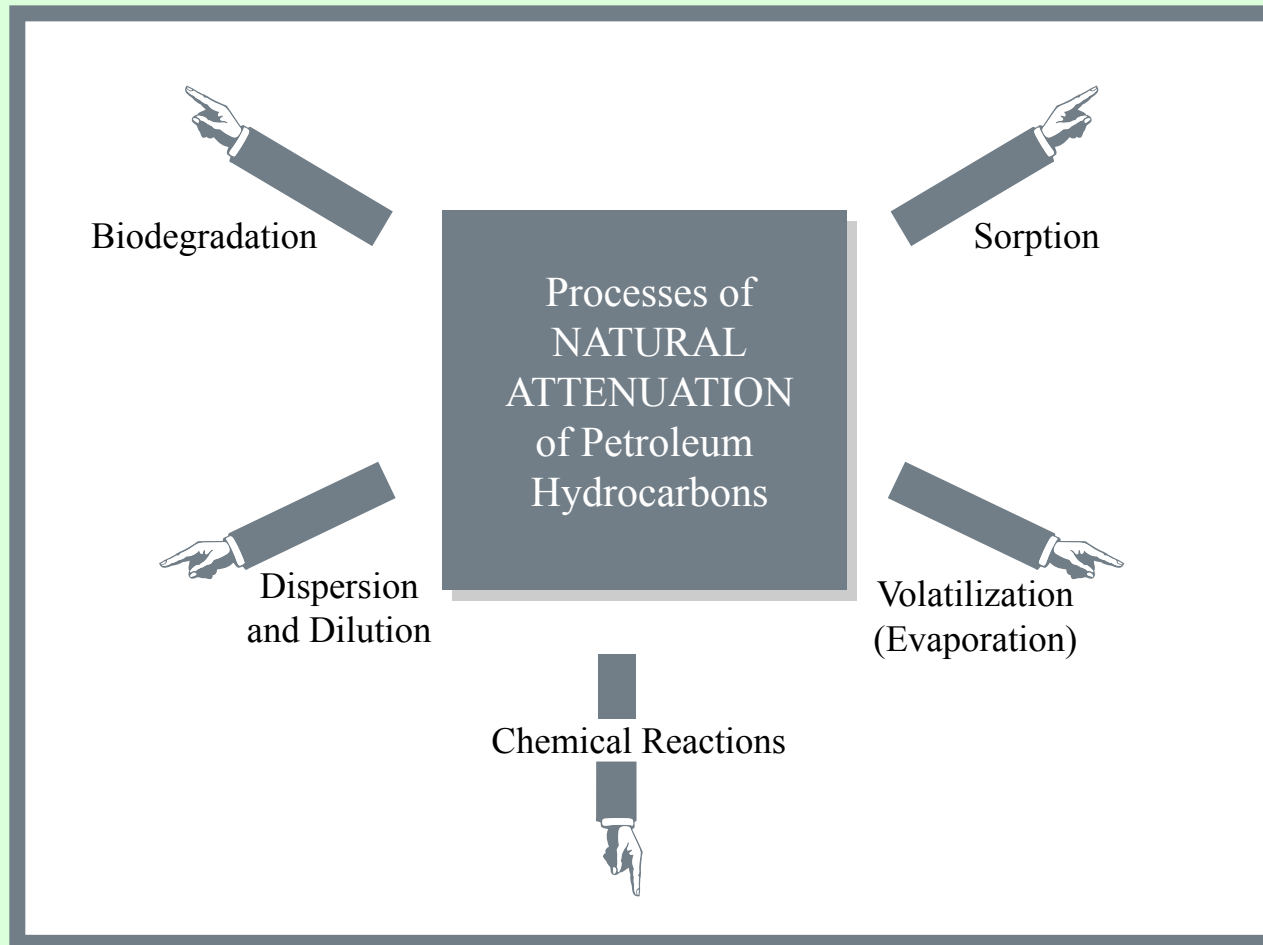
LECTURE 13

MONITORED NATURAL ATTENUATION

Monitored Natural Attenuation

As defined by U.S. EPA:

reliance on natural processes to achieve
site-specific remedial objectives



Historical development of MNA

Historical development

- 1985 – Always a remedial alternative: EPA says it was used in Superfund as early as 1985
- 1988 – Guidance on Remedial Actions for Contaminated Ground Water at Superfund Sites discusses natural attenuation, but mostly as a comparison standard for active remediation. Natural attenuation is not encouraged
- Began to be more commonplace with recognition of intractability of DNAPL cleanups and inadequacy of pump and treat technology
- Simultaneously, there was increasing recognition that in situ processes were containing or cleaning up contamination
- 1993-94 – Two key studies by National Research Council:
 - *In Situ Bioremediation – When does it work?* – 1993 study discusses intrinsic bioremediation
 - *Alternatives for Ground Water Cleanup* – 1994
- 1995 – Technical Protocol for Implementing Intrinsic Remediation with Long-Term Monitoring for Natural Attenuation of Fuel Contamination Dissolved in Groundwater
 - Prepared by Air Force Center for Environmental Excellence working with U.S. EPA research laboratory
 - Defines procedure to show intrinsic remediation is occurring
- September 1996 – EPA Symposium on Natural Attenuation of Chlorinated Organics in Ground Water
- November 1996 – Draft Technical Protocol for Evaluating Natural Attenuation of Chlorinated Solvents in Groundwater (Final in Sept. 1998)
- December 1997 – OSWER Policy Directive: Use of Monitored Natural Attenuation at Superfund, RCRA Corrective Action, and Underground Storage Tank Sites
- Sept.-Dec. 1998 – EPA Seminars on Monitored Natural Attenuation in nine cities around the US

1988 Guidance on Ground Water

United States
Environmental Protection
Agency

Office of Emergency and
Remedial Response
Washington DC 20460

EPA/540/G-88/003
OSWER Directive 9283.1-2
December 1988

Superfund



Guidance on Remedial Actions for Contaminated Ground Water at Superfund Sites

1993 and 1994 – NRC Studies

"In Situ Bioremediation. When does it work?"
National Research Council.

"Alternatives for Ground Water Cleanup." National
Research Council.

1995 – AFCEE Technical Protocol

Technical Protocol for Implementing Intrinsic
Remediation with Long-Term Monitoring for Natural Attenuation
of Fuel Contamination Dissolved in Groundwater

Volume 1

By

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Air Force Center for Environmental Excellence
Technology Transfer Division
Brooks AFB, San Antonio, Texas

Air Force Center for Environmental Excellence
Technology Transfer Division
Brooks AFB, San Antonio, Texas

1996 – EPA Symposium on Natural Attenuation

United States
Environmental Protection
Agency

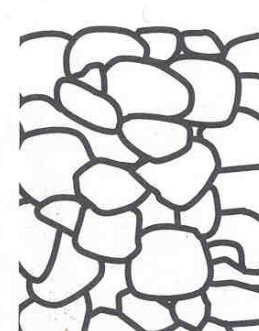
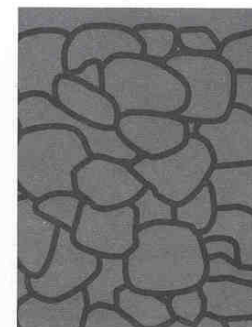
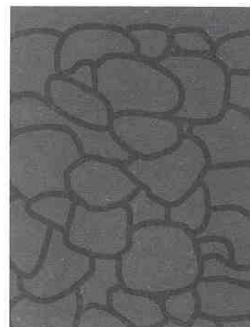
Office of Research and
Development
Washington, DC 20460

EPA/540/R-96/509
September 1996



Symposium on Natural Attenuation of Chlorinated Organics in Ground Water

Hyatt Regency Dallas
Dallas, TX
September 11–13, 1996



1996 – Draft Technical Protocol

United States
Environmental Protection
Agency

Office of Research and
Development
Washington DC 20460

EPA/600/R-98/128
September 1998



Technical Protocol for Evaluating Natural Attenuation of Chlorinated Solvents in Ground Water



Nov. 1996 – Draft

Sept. 1998 - Final

1997 – MNA Policy Directive

United States
Environmental Protection
Agency

Office of
Solid Waste and
Emergency Response



DIRECTIVE NUMBER:	9200.4-17
TITLE:	Use of Monitored Natural Attenuation at Superfund, RCRA Corrective Action, and Underground Storage Tank Sites
APPROVAL DATE:	December 1, 1997
EFFECTIVE DATE:	December 1, 1997
ORIGINATING OFFICE:	OSWER
<input type="checkbox"/> FINAL	
<input checked="" type="checkbox"/> DRAFT	Interim Final
STATUS:	
REFERENCE (other documents):	

OSWER OSWER OSWER
DIRECTIVE DIRECTIVE DIRECTIVE

1998 – MNA Seminars



Seminars

Monitored Natural Attenuation for Ground Water

September 2–3, 1998—Philadelphia, PA

September 14–15, 1998—Denver, CO

September 16–17, 1998—Chicago, IL

October 14–15, 1998—Kansas City, MO

November 2–3, 1998—Dallas, TX

November 16–17, 1998—Atlanta, GA

December 2–3, 1998—Seattle, WA

December 8–9, 1998—Boston, MA

December 14–15, 1998—San Francisco, CA

Definition of MNA (continued)

May be physical, chemical or biological

Act without human intervention to reduce the mass, toxicity, mobility, volume, or concentration of contaminants in soil or ground water

Processes include:

- biodegradation

- dispersion

- dilution

- sorption

- volatilization

- chemical or biological stabilization, transformation, or destruction

Elements of Natural Attenuation

MNA is **not**:

- No-action alternative

- Presumptive or default remedy

MNA must be:

- Evaluated along with other alternatives

- Selected only if it meets remediation objectives

- Work in reasonable time frame (30 years)

- Used very cautiously as sole remedy

Components of MNA

Required components of MNA:

- Source control

- Performance monitoring

Prerequisite for MNA:

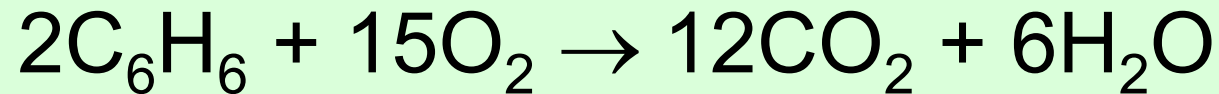
- Site-specific characterization data and analysis

Demonstrating efficacy of MNA

1. Historical chemical data showing clear trend of decreasing mass or concentration.
2. Hydrogeologic or geochemical data that indirectly demonstrate natural attenuation processes
3. Field or microcosm studies that directly demonstrate natural attenuation processes

Aerobic biodegradation of fuel hydrocarbons

Oxygen used as electron acceptor



Indicators of biodegradation:

Reduction in dissolved oxygen

(3 mg DO needed to metabolize 1 mg of benzene)

Reduction in hydrocarbon concentration

Biodegradation sequence

Order of aerobic biodegradation:

Ethyl benzene

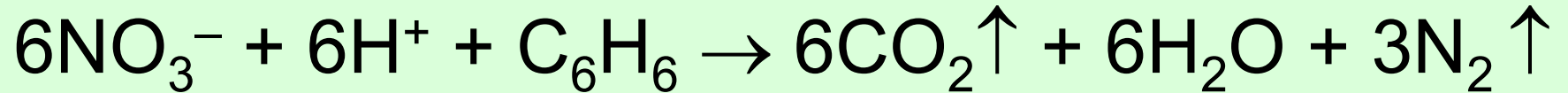
Toluene

Benzene

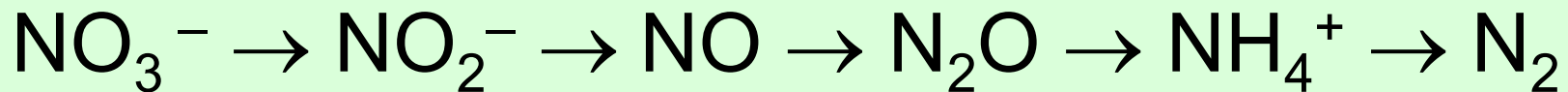
Xylene

Denitrification

Nitrate is electron acceptor



Actually occurs in multiple steps mediated by different bacteria:



Denitrification

Indicators of biodegradation:

Reduction in nitrate

Reduction in hydrocarbon concentration

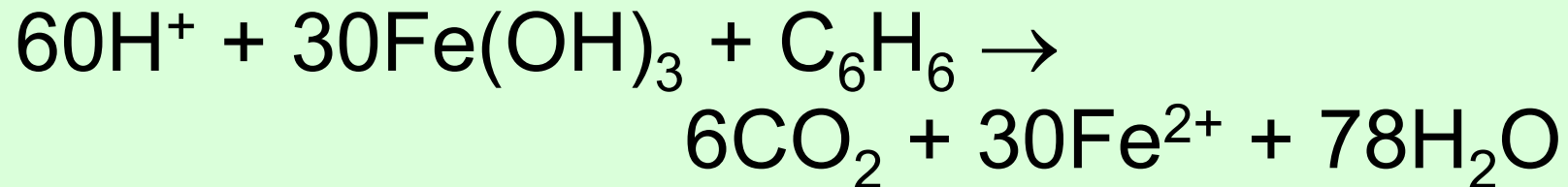
Presence of denitrifying bacteria

Reducing conditions (dissolved oxygen < 1 mg/L)

Iron reduction

Insoluble iron(III) (ferric iron) is electron acceptor

Reduced to soluble iron(II) (ferrous iron)



Iron reduction

Indicators of iron biodegradation:

Increase in dissolved iron

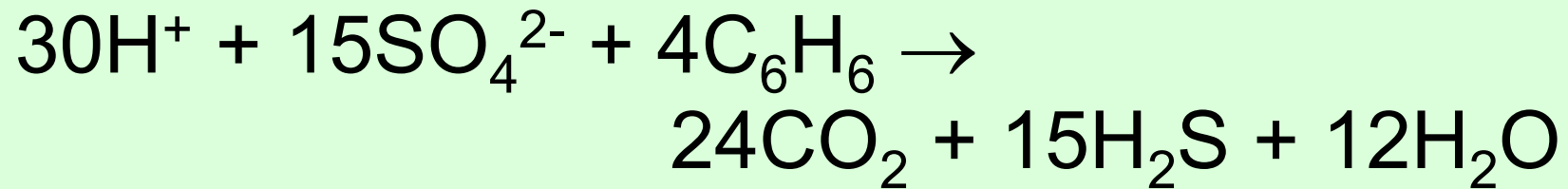
Reduction in hydrocarbon concentration

Low or no dissolved oxygen

Sulfate reduction

Sulfate is electron acceptor

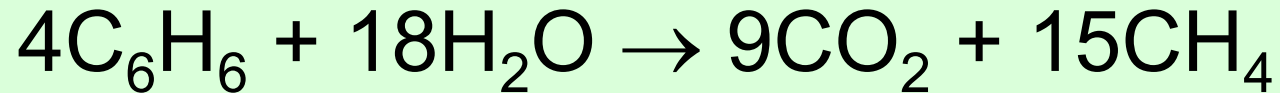
Sulfate reduction to sulfide



Methanogenesis (Methane fermentation)

Not a redox reaction – fermentation reaction

Occurs only in highly anaerobic conditions



Methanogenesis

Indicators of methanogenesis:

Increase in methane and carbon dioxide

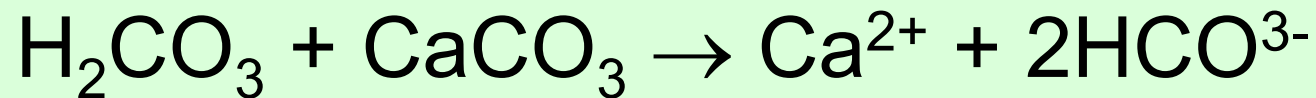
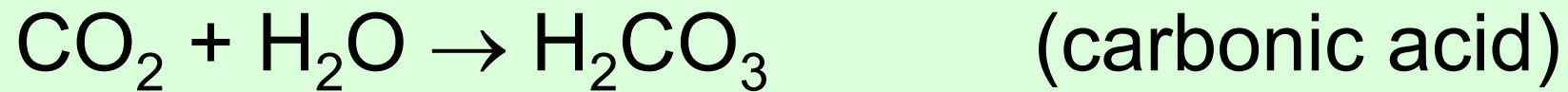
Reduction in hydrocarbon concentration

Very low or no dissolved oxygen

Presence of methanogenic bacteria

Carbon dioxide neutralization

All hydrocarbon degradation processes create CO_2



CO_2 neutralization increases alkalinity

8 mg alk produced per mg benzene degraded

Analytical protocol

Ground water:

Total hydrocarbons – confirm HC decrease

Aromatic hydrocarbons – confirm BTEX decrease

Oxygen – confirm utilization, redox state

Nitrate – confirm utilization

Iron(II) – confirm production

Sulfate – confirm utilization

Methane – confirm methanogenesis

Analytical protocol

Ground water:

Alkalinity – confirm CO₂ production and neutralization

Oxidation-reduction potential – confirm geochemical environment

pH, temperature, conductivity, chloride – confirmation of single ground-water system

Analytical protocol

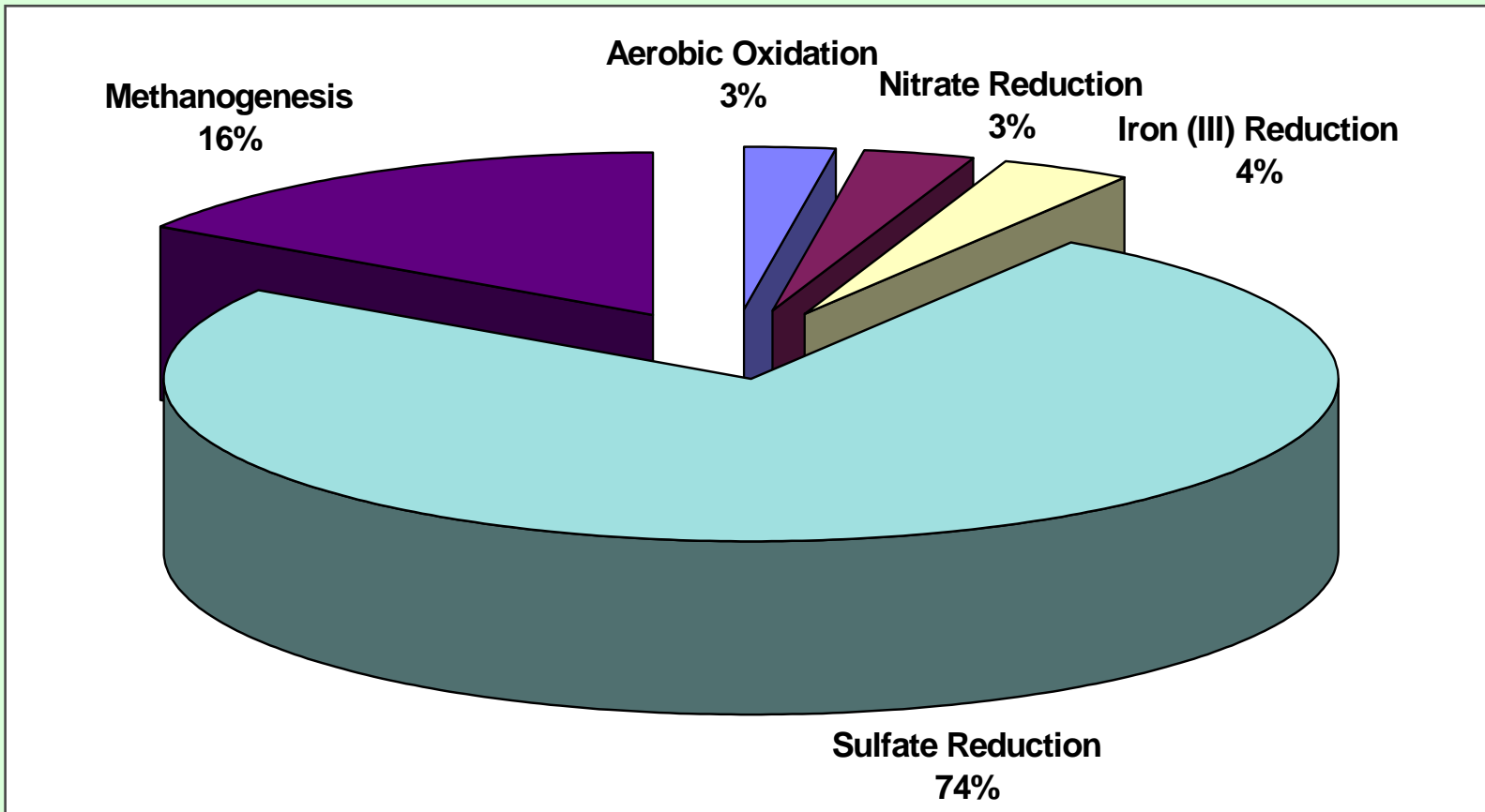
Biological:

Field dehydrogenase test – confirm presence of aerobic bacteria

Volatile fatty acids – biodegradation byproduct of complex organic compounds

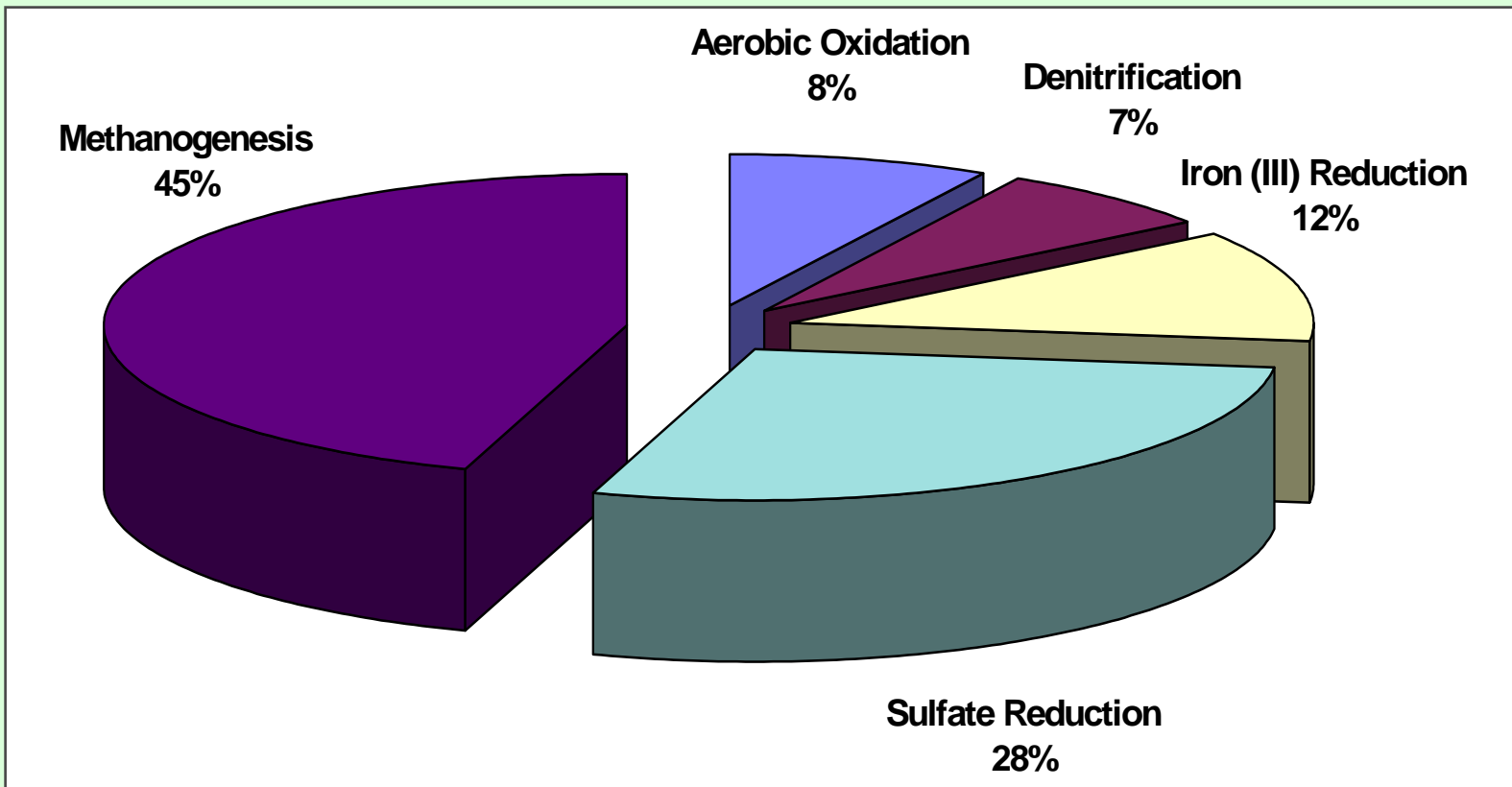
Microcosm studies – confirm biodegradation is occurring

Average Relative Contribution of BTEX Biodegradation Processes in Site Ground Water at 42 sites



Average Relative Contribution of BTEX Biodegradation Processes in Site Ground Water at 42 sites

(Excluding five sites with >200 mg/L Sulfate Reduction Capacity)



Treatability Study Results (continued)

BTEX assimilative capacity averaged 64 mg/L

Field-scale biodegradation half-lives:

Range = 9 days to 9.5 years

Mean = 1 year.



BIOSCREEN

BIOSCREEN Natural Attenuation Decision Support System

Air Force Center for Environmental Excellence

Version 1.3

Hill AFB
UST Site 870
Run Name

Data Input Instructions:

- 115 → 1. Enter value directly....or
- ↑ or 0.02 → 2. Calculate by filling in grey cells below. (To restore formulas, hit button below).
- Variable* → Data used directly in model.
- 20 → Value calculated by model. (Don't enter any data).

1. HYDROGEOLOGY

Seepage Velocity*	Vs	1609.1	(ft/yr)
or			
Hydraulic Conductivity	K	8.1E-03	(cm/sec)
Hydraulic Gradient	i	0.048	(ft/ft)
Porosity	n	0.25	(-)

2. DISPERSION

Longitudinal Dispersivity*	alpha x	28.5	(ft)
Transverse Dispersivity*	alpha y	2.9	(ft)
Vertical Dispersivity*	alpha z	0.0	(ft)
or			
Estimated Plume Length	Lp	1450	(ft)

3. ADSORPTION

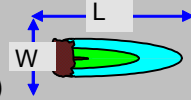
Retardation Factor*	R	1.2	(-)
or			
Soil Bulk Density	rho	1.7	(kg/l)
Partition Coefficient	Koc	38	(L/kg)
Fraction Organic Carbon	foc	8.00E-04	(-)

4. BIODEGRADATION

1st Order Decay Coeff*	lambda	6.9E+0	(per yr)
or			
Solute Half-Life	t-half	0.10	(year)
or Instantaneous Reaction Model			
Delta Oxygen*	DO	5.78	(mg/L)
Delta Nitrate*	NO3	17	(mg/L)
Observed Ferrous Iron*	Fe2+	11.3	(mg/L)
Delta Sulfate*	SO4	100	(mg/L)
Observed Methane*	CH4	0.414	(mg/L)

5. GENERAL

Modeled Area Length*	1450	(ft)
Modeled Area Width*	320	(ft)
Simulation Time*	5	(yr)



6. SOURCE DATA

Source Thickness in Sat.Zone* 100 (ft)

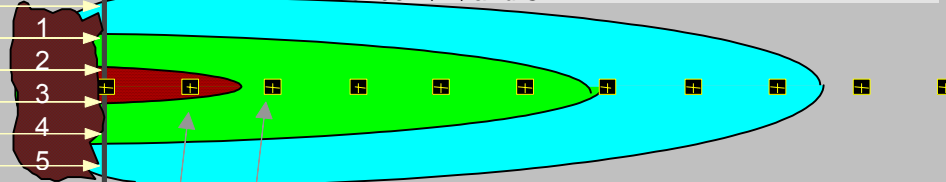
Source Zones:
Width* (ft) | Conc. (mg/L)*

50	0.07
25	2.8
100	9
25	2.8
50	0.07

Source Decay (see Help):

SourceHalfLife*	Infinite	(yr)
Soluble Mass	↑ or	
In NAPL, Soil	Infinite	(Kg)

Vertical Plane Source: Look at Plume Cross-Section and Input Concentrations & Widths for Zones 1, 2, and 3



View of Plume Looking Down

Observed Centerline Concentrations at Monitoring Wells
If No Data Leave Blank or Enter "0"

7. FIELD DATA FOR COMPARISON

Concentration (mg/L)	90		8.0				1.0		.02	.005	
Dist. from Source (ft)	0	145	290	435	580	725	870	1015	1160	1305	1450

8. CHOOSE TYPE OF OUTPUT TO SEE:

RUN CENTERLINE

RUN ARRAY

Help

Recalculate This Sheet

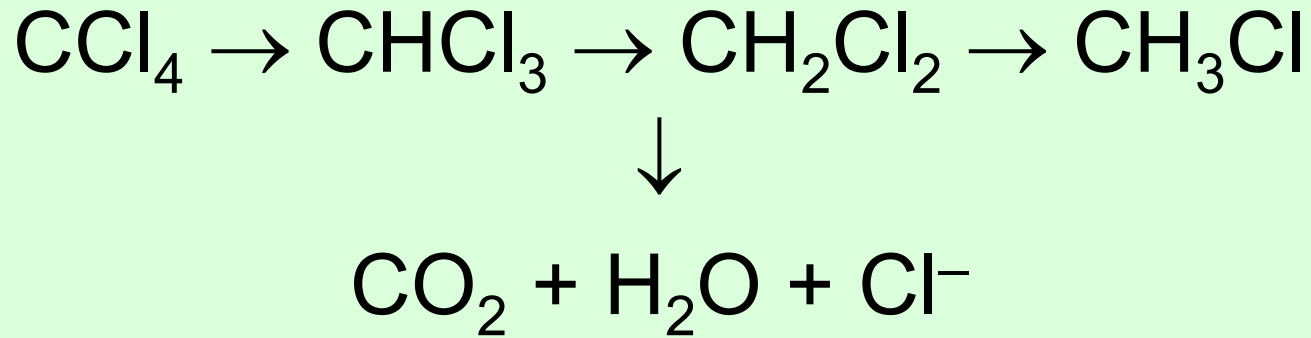
View Output

View Output

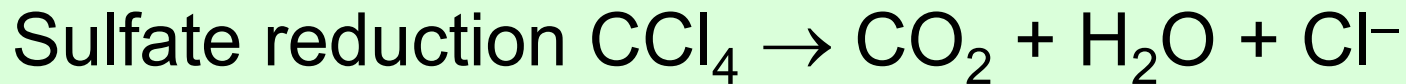
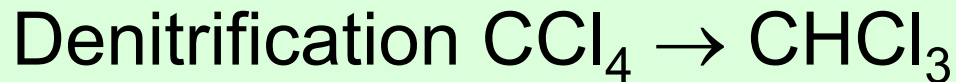
Paste Example Dataset

Restore Formulas for Vs, Dispersivities, R, lambda, other

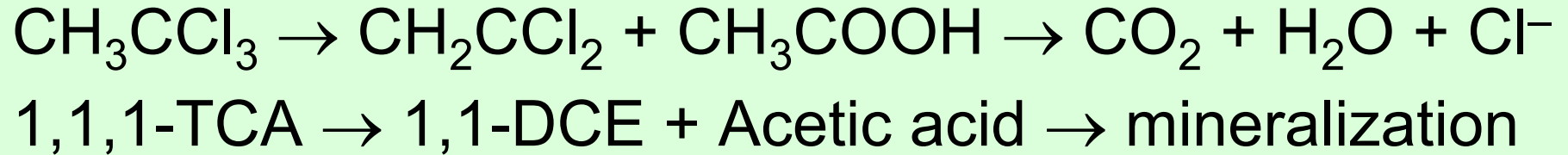
Anaerobic transformation of carbon tetrachloride



Redox conditions:



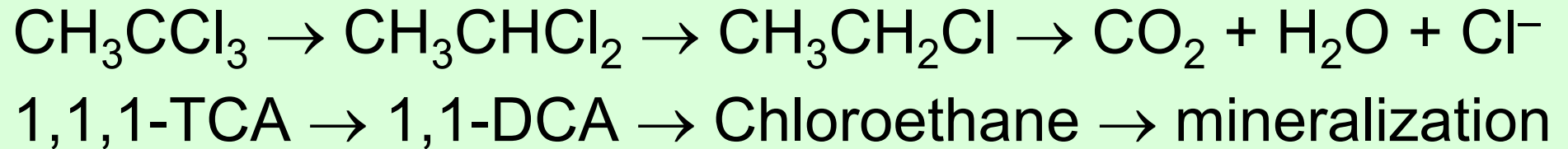
Abiotic degradation of TCA



Redox conditions:

All redox conditions

Anaerobic dechlorination of TCA

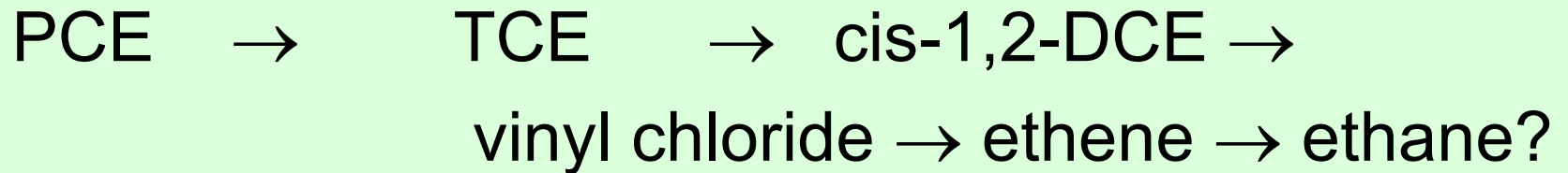
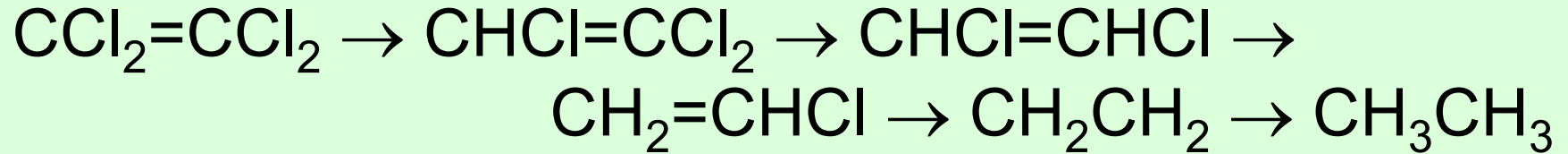


Redox conditions:

Sulfate reduction 1,1,1-TCA → 1,1-DCA

Methanogenesis 1,1,1-TCA → mineralization

Anaerobic degradation of PCE & TCE



Redox conditions:

Sulfate reduction PCE \rightarrow DCE, TCE \rightarrow DCE

Methanogenesis PCE \rightarrow ethene, TCE \rightarrow ethene

Analytical protocol

Ground water:

Same as for hydrocarbons, plus:

Methane – to confirm methanogenesis

Chlorinated VOCs – materials degraded and degradation products

Distinguish cis-1,2-DCE and trans-1,2-DCE

Degradation byproducts: CO₂, ethane, ethene, chloride

Analytical protocols

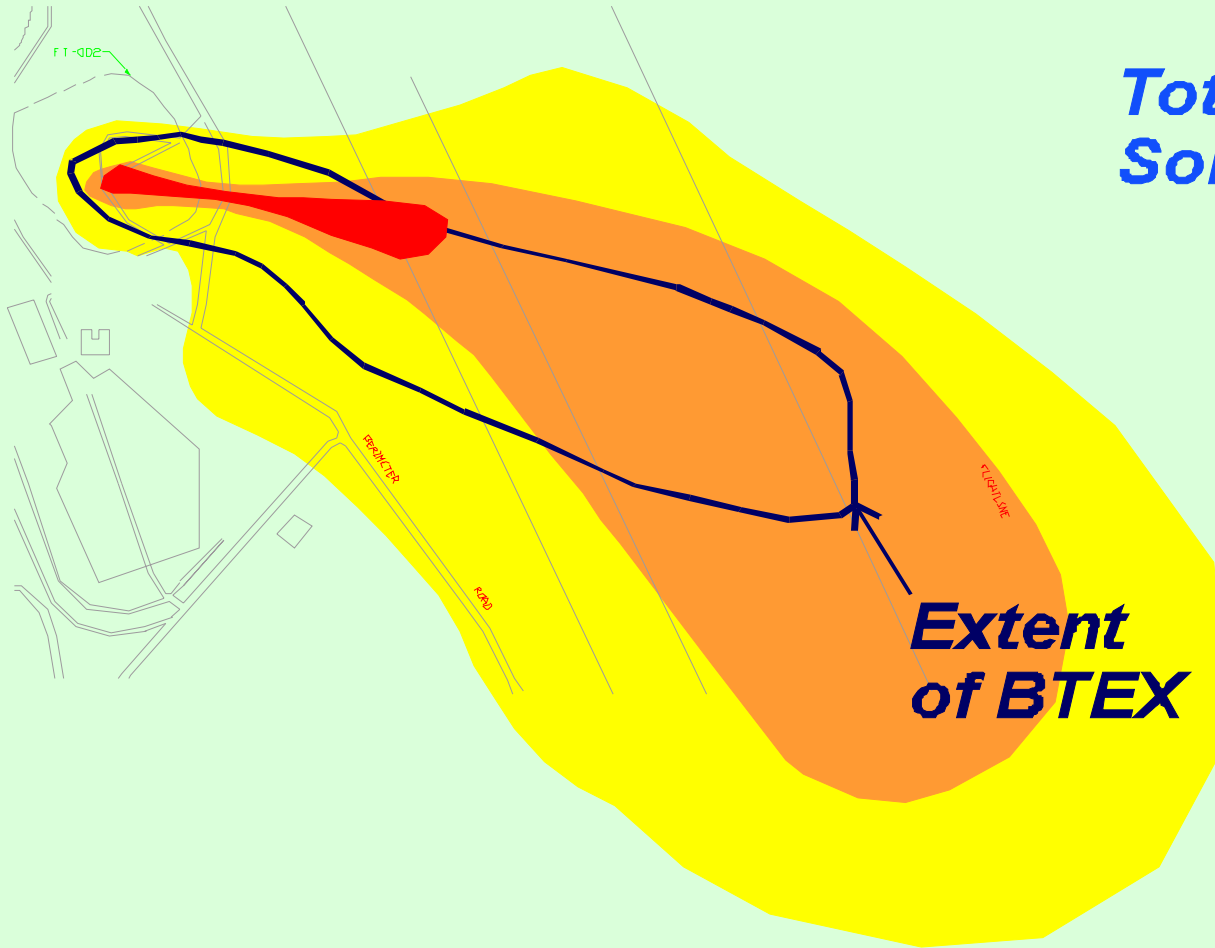
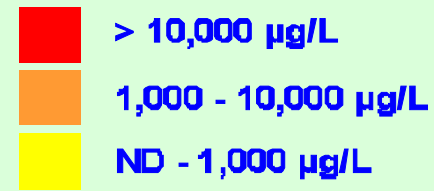
Ground water:

Dissolved hydrogen – distinguishes strength of dechlorination and redox state:

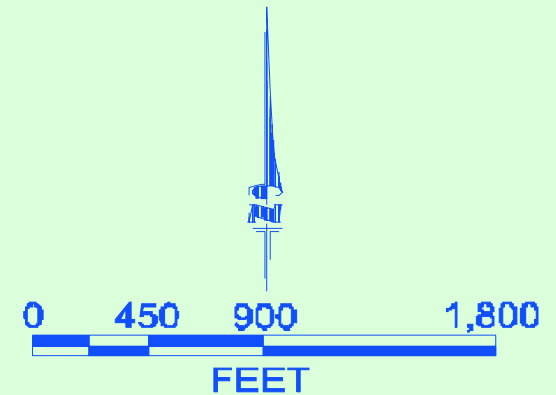
Electron acceptor	H₂ concentration (ng/L)
Denitrification	< 0.1
Iron reduction	0.2 to 0.8
Sulfate reduction	1 to 4
Reductive dechlorination	> 1
Methanogenesis	5 to 20

Extent of Chlorinated Solvents and BTEX

Total Chlorinated Solvent Concentration

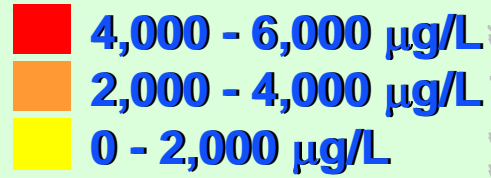
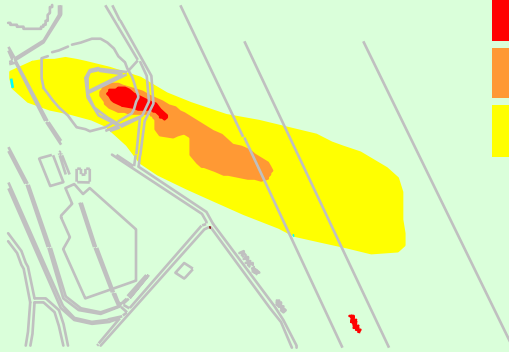


Extent of BTEX

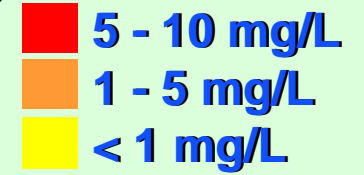
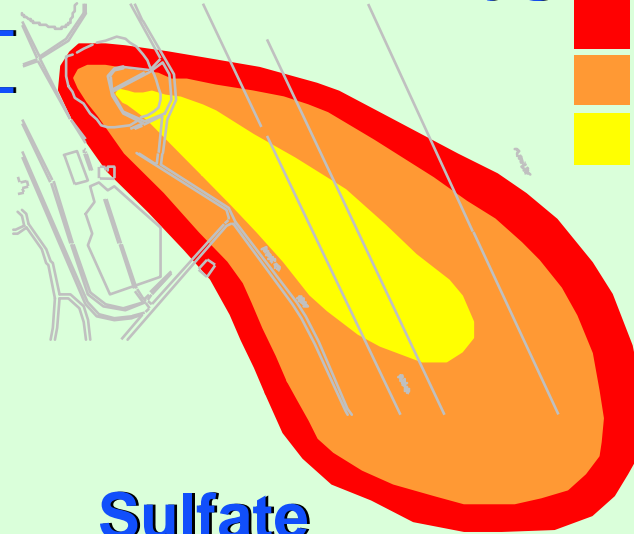


BTEX and Electron Acceptors

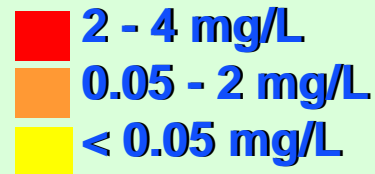
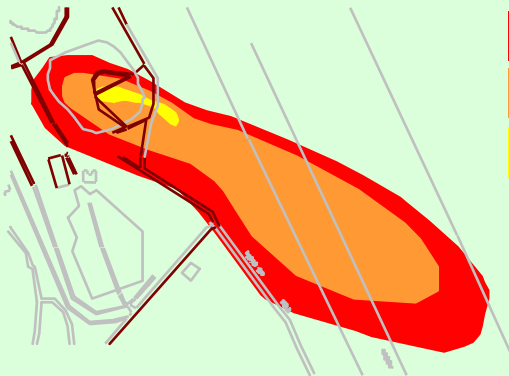
Total BTEX



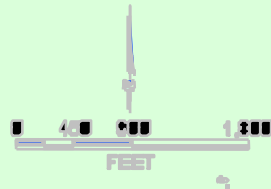
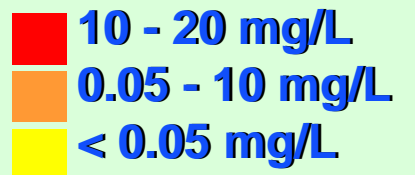
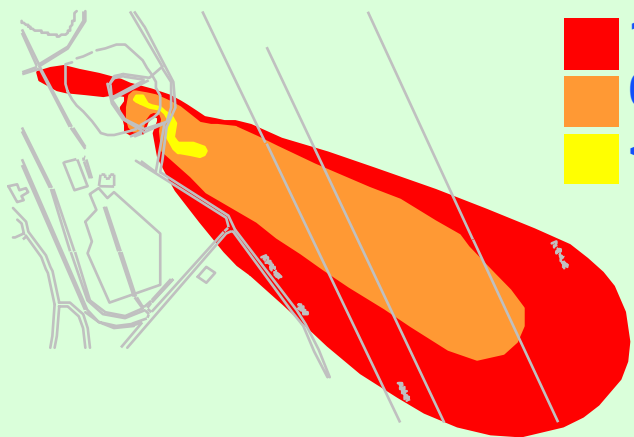
Dissolved Oxygen



Nitrate

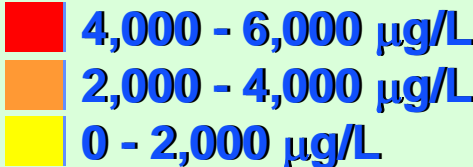
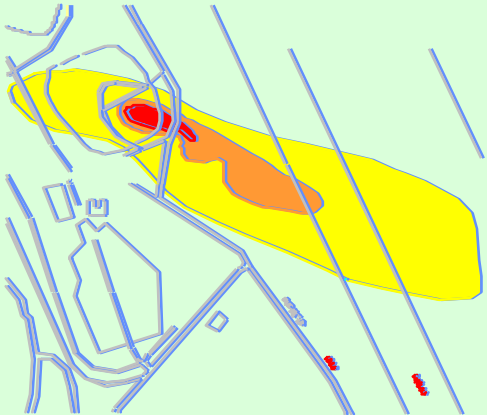


Sulfate

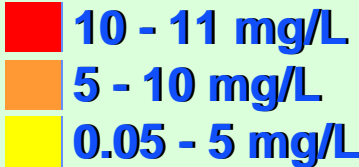
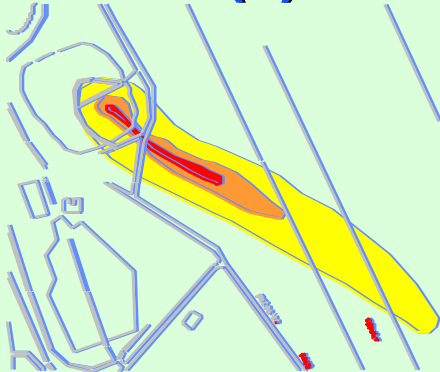


BTEX and Metabolic Byproducts

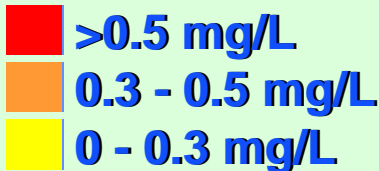
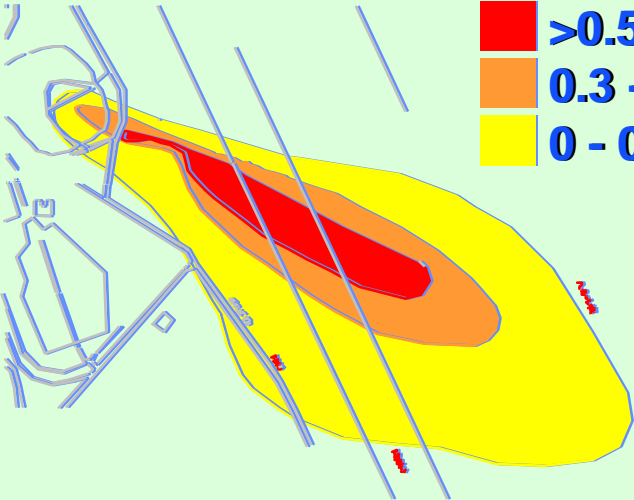
Total BTEX



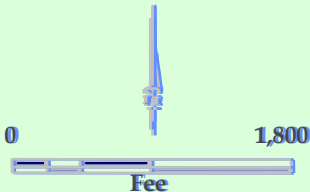
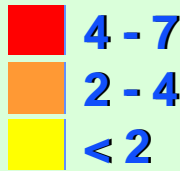
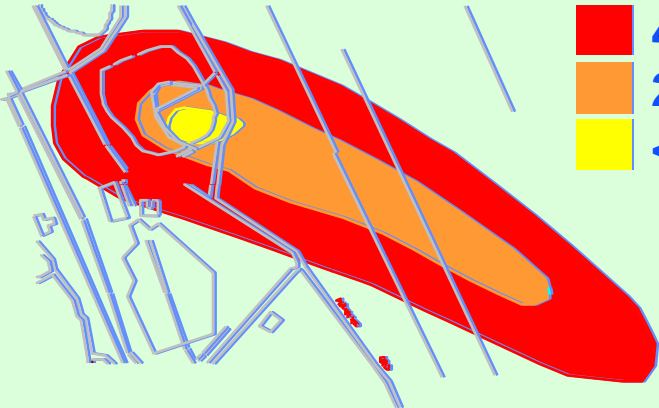
Iron (II)



Methane

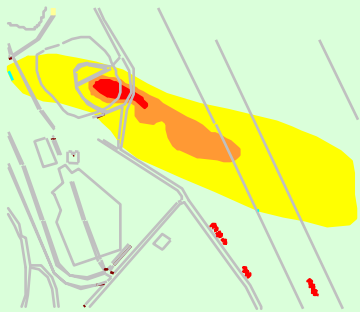


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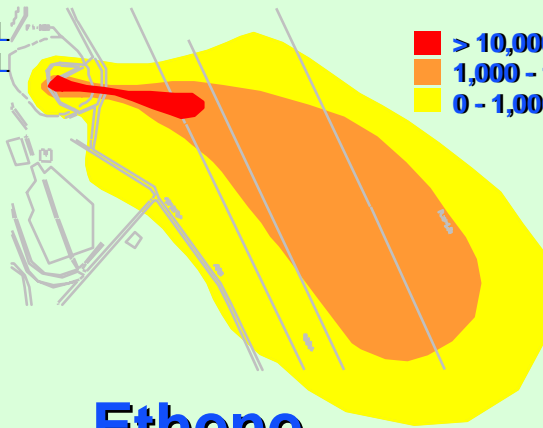
Chlorinated Solvents and Byproducts

Total BTEX



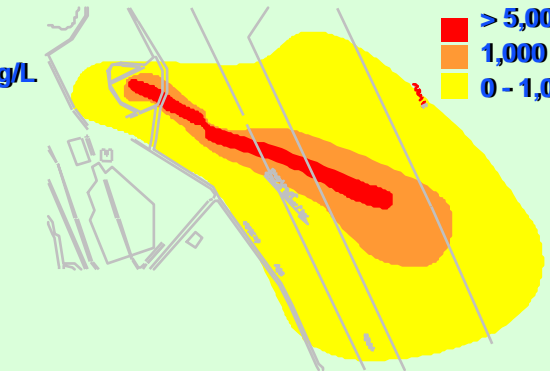
4,000 - 6,000 $\mu\text{g/L}$
2,000 - 4,000 $\mu\text{g/L}$
0 - 2,000 $\mu\text{g/L}$

Trichloroethene



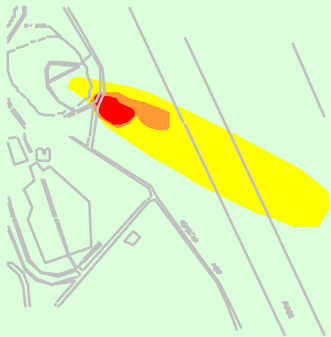
> 10,000 $\mu\text{g/L}$
1,000 - 10,000 $\mu\text{g/L}$
0 - 1,000 $\mu\text{g/L}$

Dichloroethene



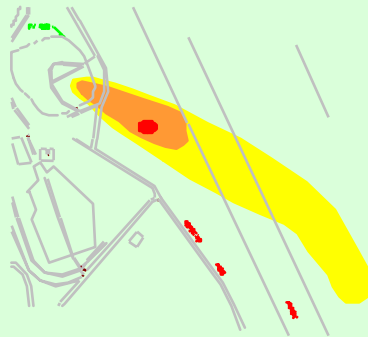
> 5,000 $\mu\text{g/L}$
1,000 - 5,000 $\mu\text{g/L}$
0 - 1,000 $\mu\text{g/L}$

Vinyl Chloride



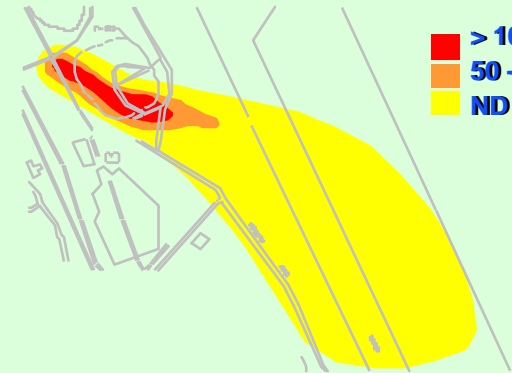
> 1,000 $\mu\text{g/L}$
500 - 1,000 $\mu\text{g/L}$
ND - 500 $\mu\text{g/L}$

Ethene

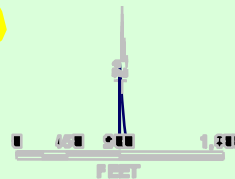


> 500 $\mu\text{g/L}$
100 - 500 $\mu\text{g/L}$
ND - 100 $\mu\text{g/L}$

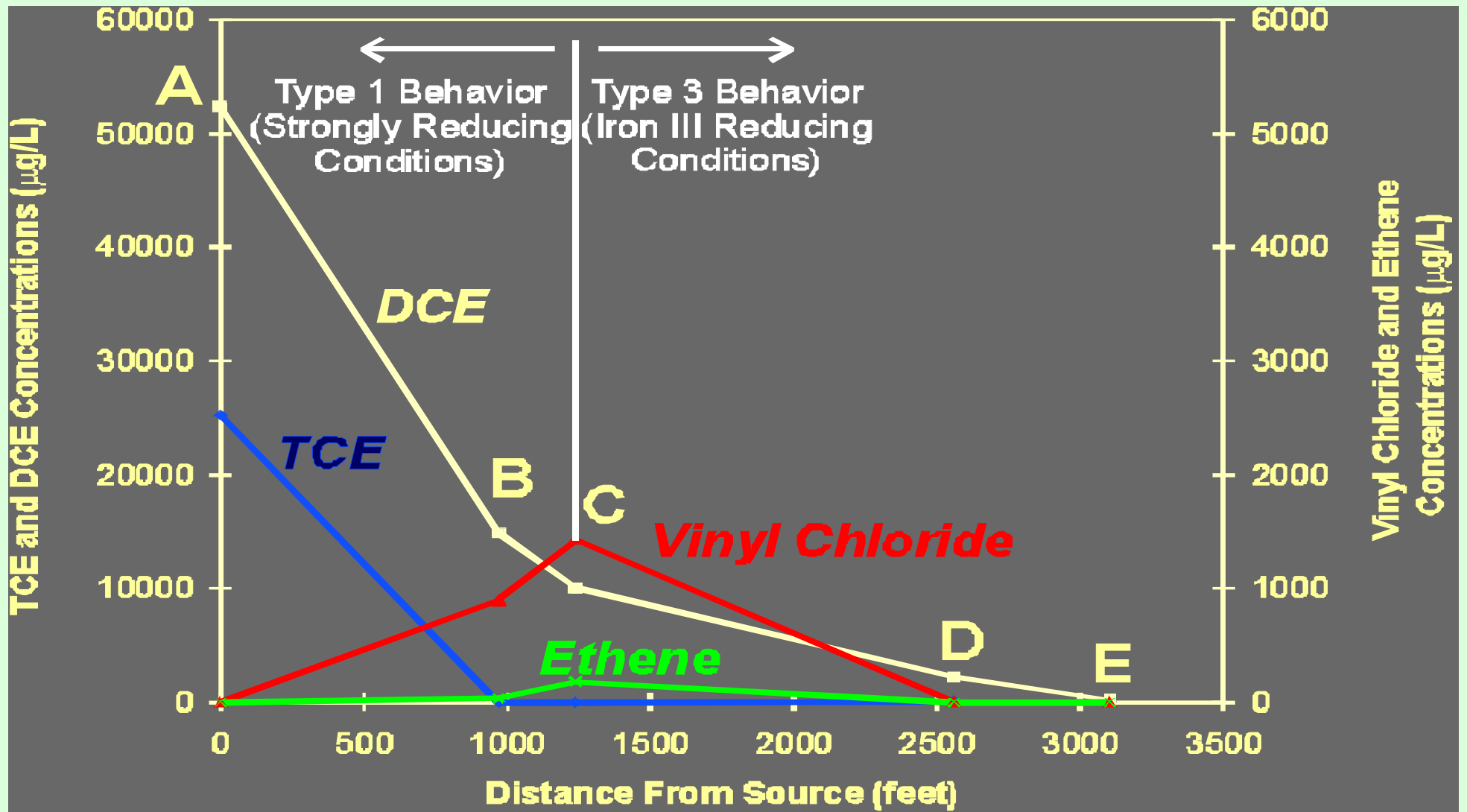
Chloride



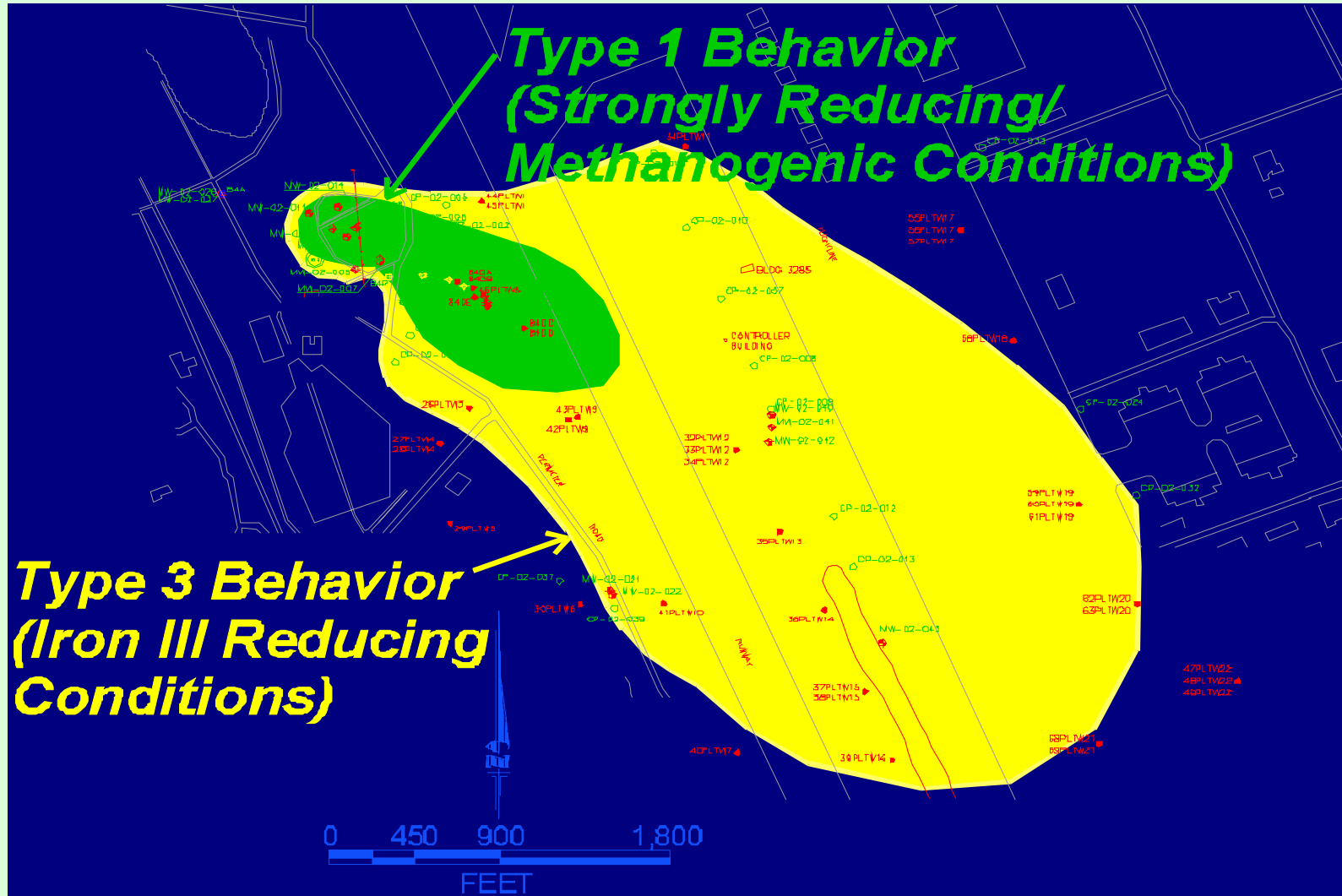
> 100 mg/L
50 - 100 mg/L
ND - 50 mg/L

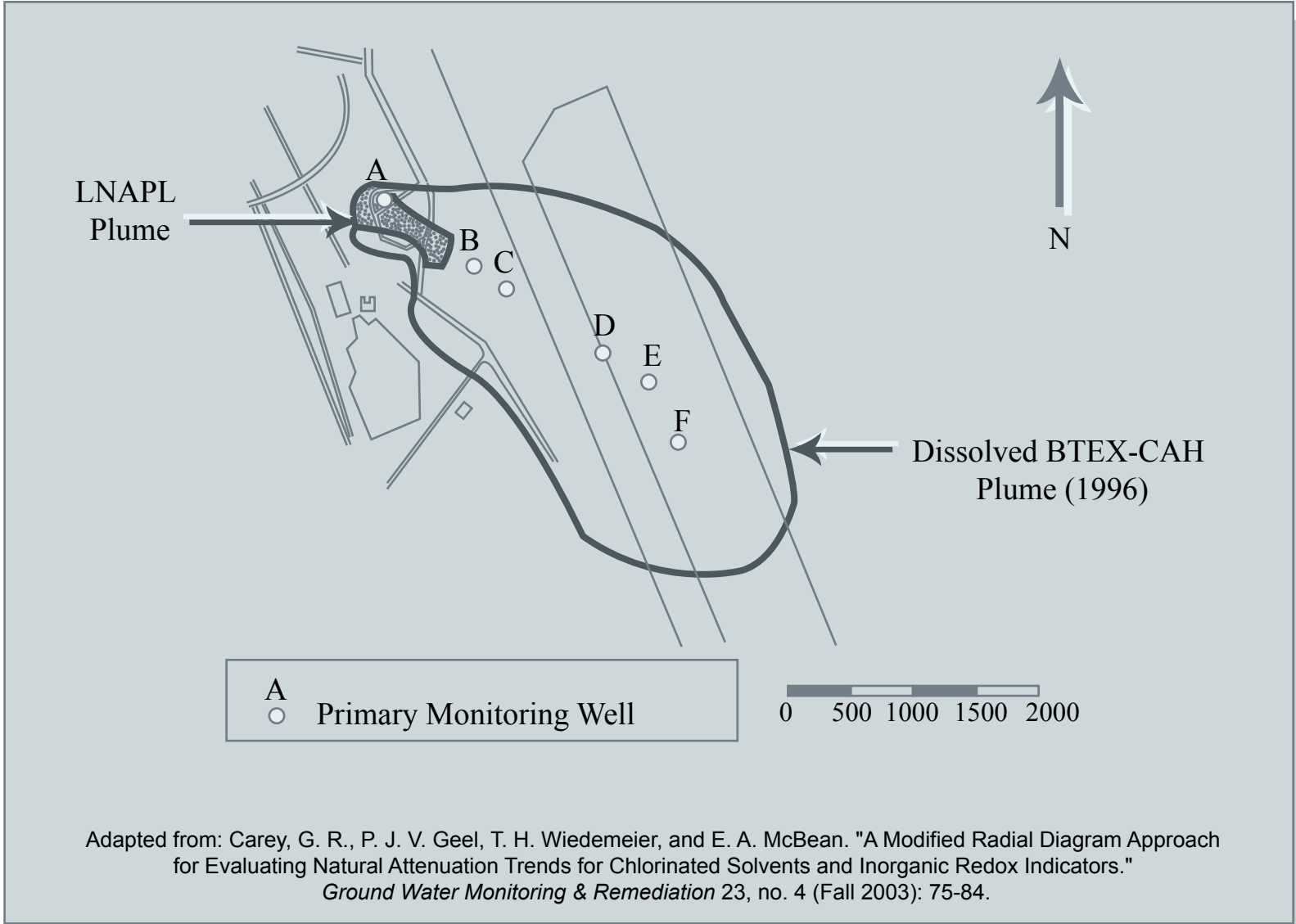


Plot of TCE, DCE, VC, and Ethene versus Distance Downgradient

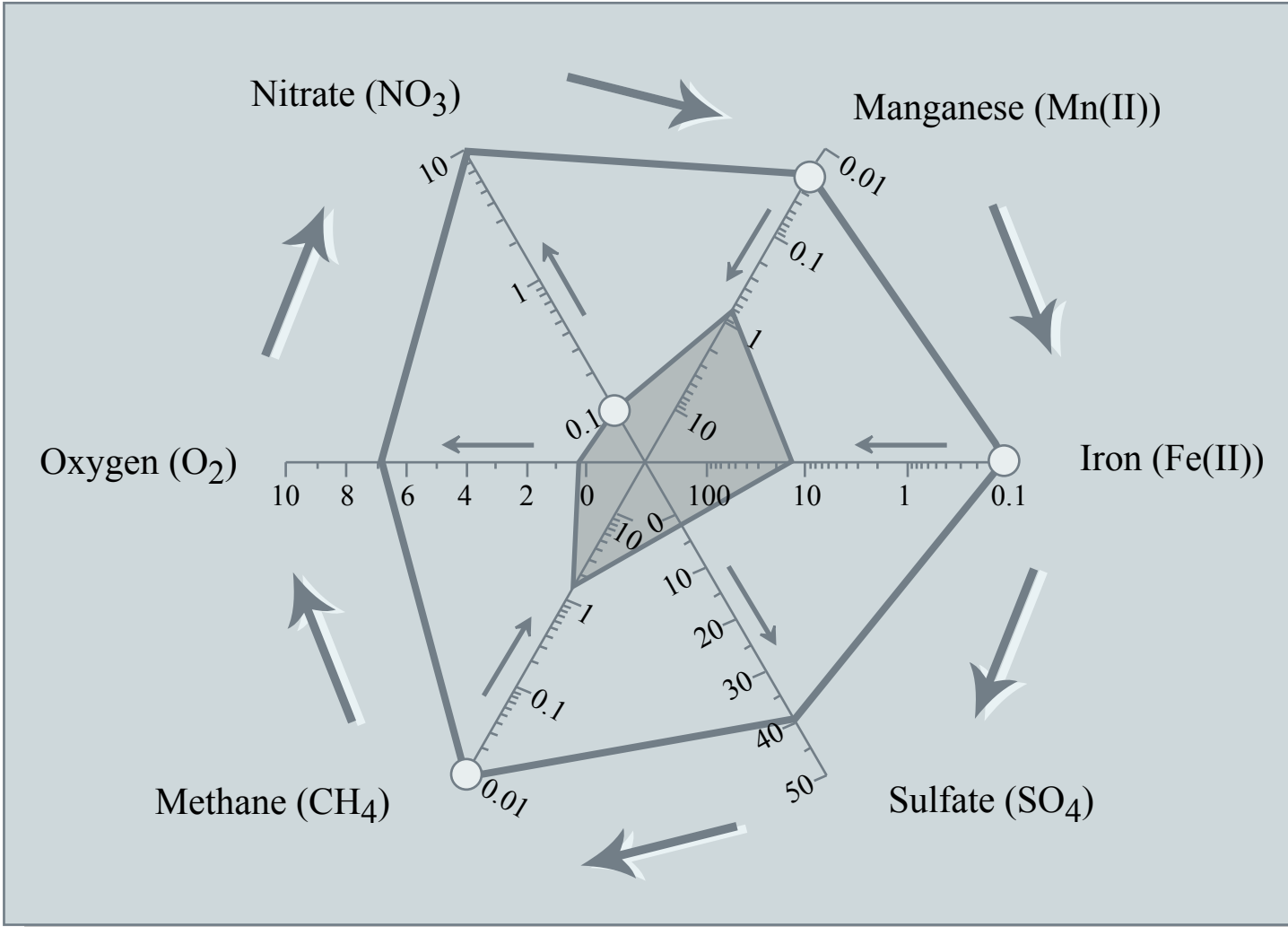


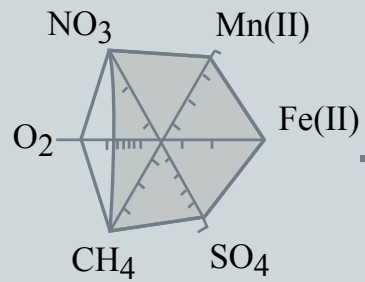
Plume Classification



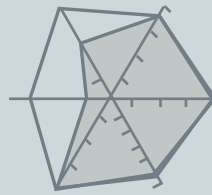


Adapted from: Carey, G. R., P. J. V. Geel, T. H. Wiedemeier, and E. A. McBean. "A Modified Radial Diagram Approach for Evaluating Natural Attenuation Trends for Chlorinated Solvents and Inorganic Redox Indicators." *Ground Water Monitoring & Remediation* 23, no. 4 (Fall 2003): 75-84.

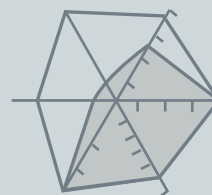




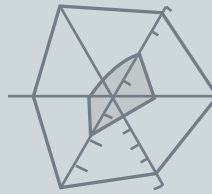
Aerobic



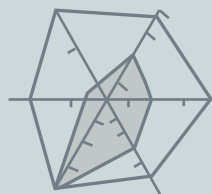
Nitrate-Reducing



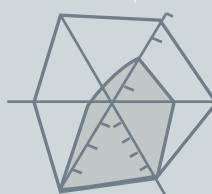
Manganogenic



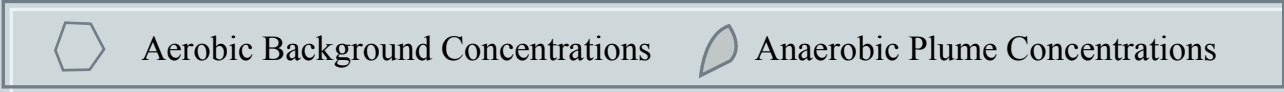
Methanogenic

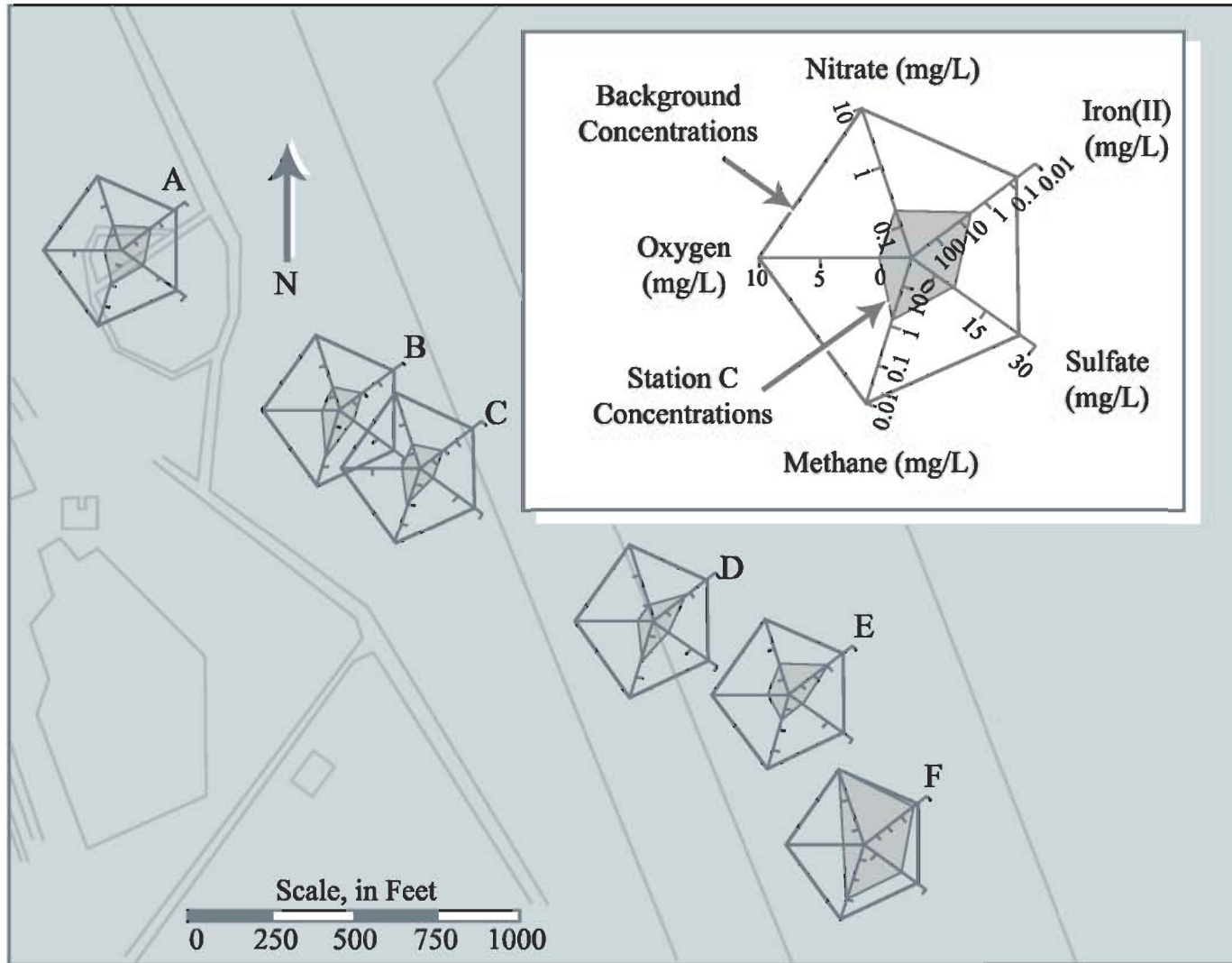


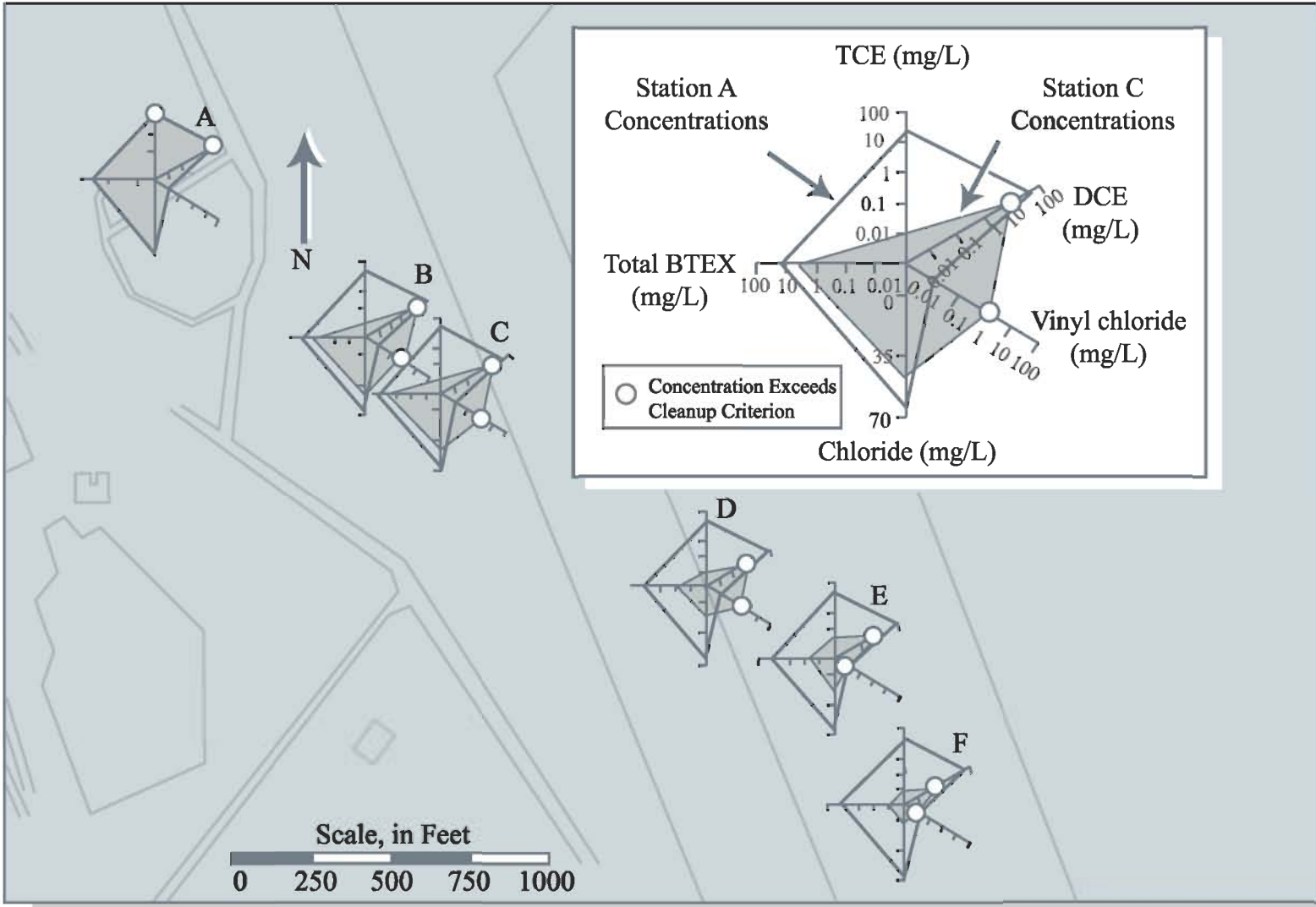
Sulfate-Reducing



Ferrogenic









BIOCHLOR

BIOCHLOR Natural Attenuation Decision Support System

Version 1.1
for Excel 7.0/ '95

Cape Canaveral
Fire Training Area
Run Name

Data Input Instructions:

1. Enter value directly...or
 2. Calculate by filling in gray cells. Press Enter, then **C**
(To restore formulas, hit "Restore Formulas" button)
- Variable* → Data used directly in model.

Test if Biotransformation is Occurring → **Natural Attenuation Screening Protocol**

TYPE OF CHLORINATED SOLVENT: Ethenes / Ethanes

1. ADVECTION

Seepage Velocity* Vs: 111.7 (ft/yr) or 0.02 (ft/yr)

Hydraulic Conductivity K: 1.8E-02 (cm/sec)

Hydraulic Gradient i: 0.0012 (ft/ft)

Effective Porosity n: 0.2 (-)

5. GENERAL

Simulation Time*: 33 (yr)

Modeled Area Width*: 700 (ft)

Modeled Area Length*: 1085 (ft)

Zone 1 Length*: 1085 (ft)

Zone 2 Length*: 0 (ft)

Zone 2 = L - Zone 1

2. DISPERSION

Alpha x Calc. Method: 40 (ft)

(Alpha y) / (Alpha x): 0.1 (-)

(Alpha z) / (Alpha x): 1.E-99 (-)

Change Alpha x Calc. Method

6. SOURCE DATA

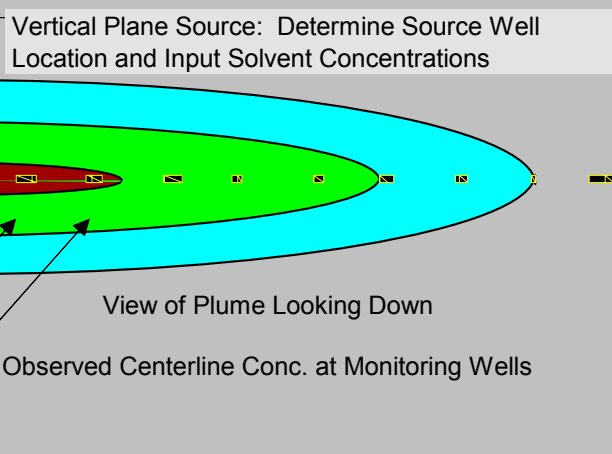
Source Options: TYPE: Single Planar

Source Thickness in Sat. Zone*: 56 (ft)

Width* (ft): 105

Conc. (mg/L)* C1

PCE	.056
TCE	15.8
DCE	98.5
VC	3.08
ETH	.03



3. ADSORPTION

Retardation Factor* R

Soil Bulk Density, rho: 1.6 (kg/L)

Fraction Organic Carbon, foc: 1.8E-3 (-)

Partition Coefficient Koc

PCE	426 (L/kg)	7.1 (-)
TCE	130 (L/kg)	2.9 (-)
DCE	125 (L/kg)	2.8 (-)
VC	30 (L/kg)	1.4 (-)
ETH	302 (L/kg)	5.3 (-)

Common R (used in model)* = 2.9

7. FIELD DATA FOR COMPARISON

PCE Conc. (mg/L)	.056									
TCE Conc. (mg/L)	15.8	.22	.0117	.024	.019					
DCE Conc. (mg/L)	98.5	3.48	.776	1.2	5.56					
VC Conc. (mg/L)	3.08	3.08	.797	2.52	5.024					
ETH Conc. (mg/L)	.03	.188		.107	.15					
Dist. from Source (ft)	0	560	650	930	1085					

4. BIOTRANSFORMATION

-1st Order Decay Coef* λ (1/yr) half-life (yrs) Yield*

Zone 1

PCE → TCE	2.00		0.79
TCE → DCE	1.00		0.74
DCE → VC	0.70		0.64
VC → ETH	0.40		0.45

Zone 2

PCE → TCE	0.00		
TCE → DCE	0.00		
DCE → VC	0.00		
VC → ETH	0.00		
ETH → Ethane			

8. CHOOSE TYPE OF OUTPUT TO SEE:

RUN CENTERLINE **RUN ARRAY**

Help **Restore Formulas** **RESET**

SEE OUTPUT **Paste Example**

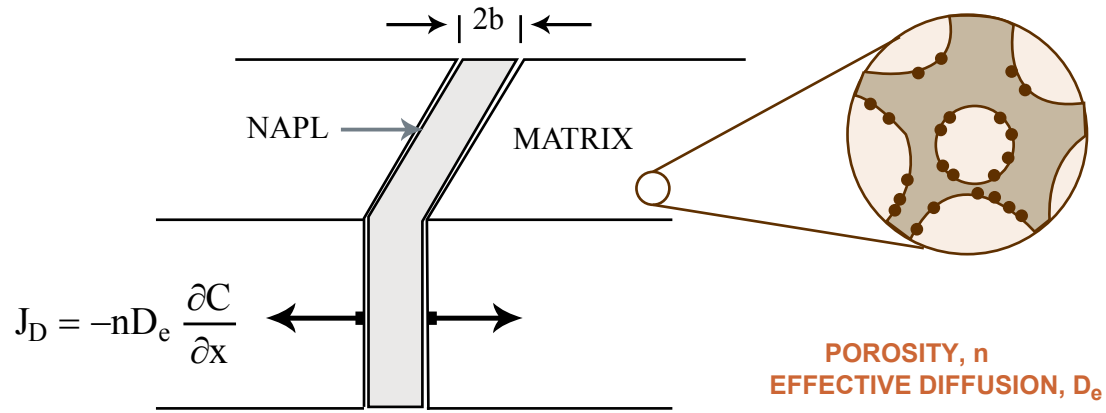
Diffusive disappearance

Parker, B. L., R. W. Gillham and J. A. Cherry, 1994.
"Diffusive Disappearance of Immiscible-Phase
Organic Liquids in Fractured Geologic Media."
Ground Water, Vol. 32, No. 5, Pp. 805-820.
September/October 1994.

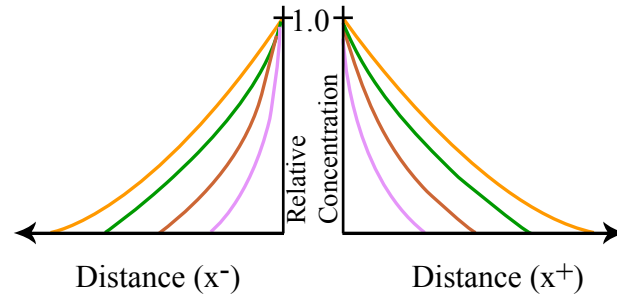
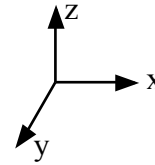
See Figure 1 of:

Parker, B. L., R. W. Gillham and J. A. Cherry, 1994. "Diffusive Disappearance of Immiscible-Phase Organic Liquids in Fractured Geologic Media." *Ground Water*, Vol. 32, No. 5, Pp. 805-820. September/October 1994.

FRACTURE APERTURE



POROSITY, n
EFFECTIVE DIFFUSION, D_e



$$J_D = -nD_e \frac{\partial C}{\partial x}$$

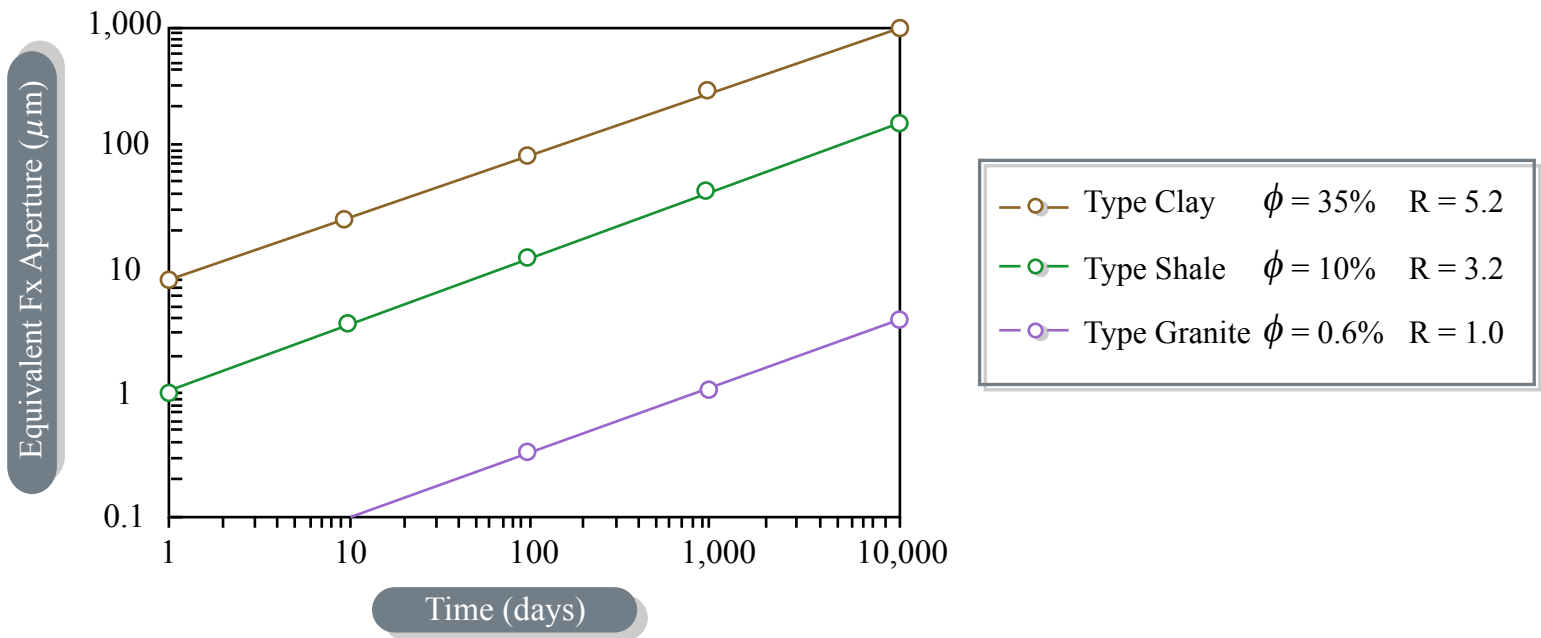
$$\frac{\partial C}{\partial t} = \frac{D_e}{R} \frac{\partial^2 C}{\partial x^2}$$

Assume $C(x = 0, t) = S_w$
and $C(x, t = 0) = 0$

$$J_D(0, t) = -nS_w \left(\frac{RD_e}{\pi t} \right)^{1/2}$$

Integrate over time to get mass leaving fracture :

$$M_t = nS_w \frac{4}{\sqrt{\pi}} (RD_e t)^{1/2}$$



Comparison of TCE mass loss rates for three geologic media expressed in terms of equivalent immiscible-phase fracture aperture and time for NAPL disappearance: type-clay $R = 5.2$, type-sandstone/shale $R = 3.2$, and type-granite $R = 1$. Parameter values provided in the next slide.

Image adapted from: Parker, B. L., R. W. Gillham and J. A. Cherry, 1994. "Diffusive Disappearance of Immiscible-Phase Organic Liquids in Fractured Geologic Media." *Ground Water*, Vol. 32, No. 5. Pp. 805-820. September/October 1994.

Geologic media parameters for three type-fractured geologic media used for comparison of TCE mass loss rates due to diffusion and sorption to matrix solids presented in figure: type-clay, type-shale/sandstone, and type-granite.

Parameter	Clay	Type-geologic media Shale/sandstone	Granite
Porosity: ϕ	0.35	0.10	0.006
Bulk density: ρ_b (g/cm ³)	1.6	2.4	2.63
Fraction organic carbon: f_{oc}	0.01	0.002	0
Apparent tortuosity: τ	0.33	0.10	0.06
		Combined parameters: TCE & geologic media	
Effective diffusion coefficient: D_e (cm ² /s)	3.3E-06	1.0E-06	6.0E-06
Retardation factor: R	5.2	3.2	1

Image adapted from: Parker, B. L., R. W. Gillham and J. A. Cherry, 1994. "Diffusive Disappearance of Immiscible-Phase Organic Liquids in Fractured Geologic Media." *Ground Water*, Vol. 32, No. 5. Pp. 805-820. September/October 1994.