

# Numerical Methods for PDEs

*Integral Equation Methods, Lecture 5*  
*First and Second Kind Potential Equations*

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# Outline

**Reminder about 1-D 1st and 2nd Kind Eqns**

**Three-D Laplace Problems**

Interior Neumann Problem

Null space issue

**First Kind Theory for 3-D Laplace**

Informal Convergence Theory

FEM like approach

# 1-D Reminder

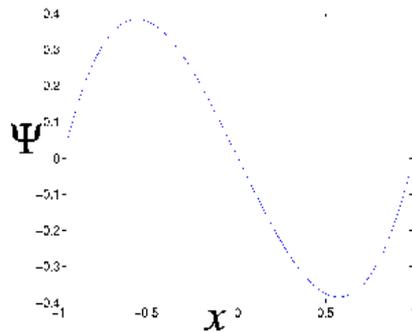
## 1st Kind Example

### First Kind Equation

$$\Psi(x) = \int_{-1}^1 |x - x'| \sigma(x') dS' \quad x \in [-1, 1]$$

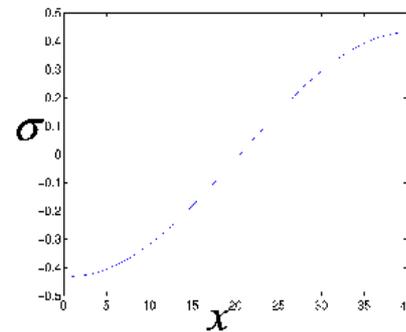
The potential is given

$$\Psi(x) = x^3 - x$$



The density must be computed

$\sigma(x)$  is unknown



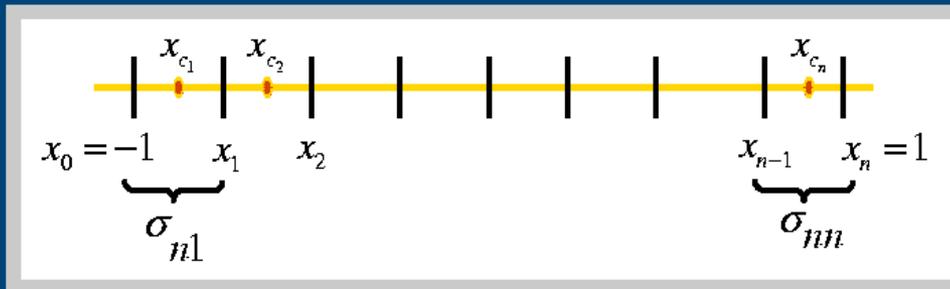
## 1st Kind Example

### 1-D Reminder

Discretization

$$\Psi(x) = \int_{-1}^1 |x - x'| \sigma(x') dS' \quad x \in [-1, 1]$$

### Centroid Collocated Piecewise Constant Scheme



$$\Psi(x_{c_i}) = \sum_{j=1}^n \sigma_{nj} \int_{x_{j-1}}^{x_j} |x_{c_i} - x'| dS'$$

# 1st Kind Example

## 1-D Reminder

Matrix

One column for each density value

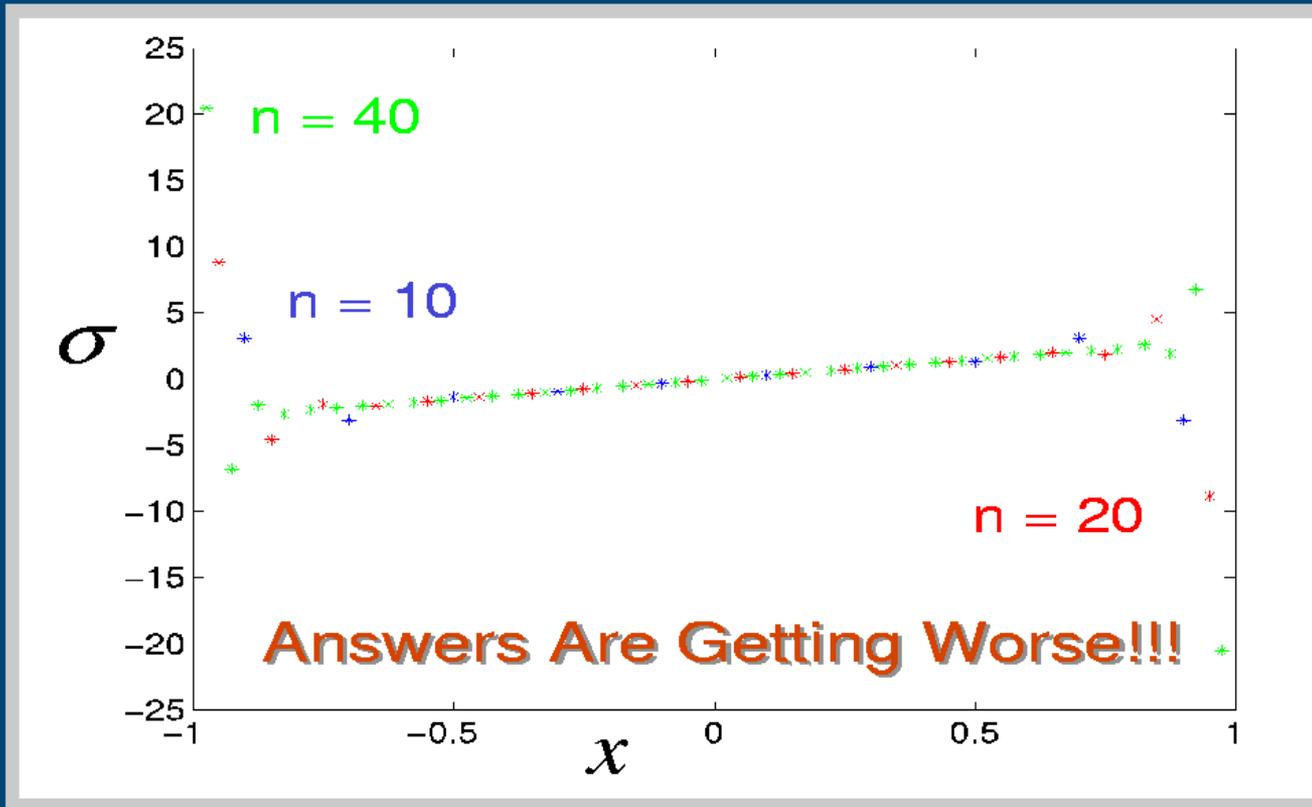
$$\begin{bmatrix} \int_{x_0}^{x_1} |x_{c_1} - x'| dS' & \cdots & \int_{x_{n-1}}^{x_n} |x_{c_1} - x'| dS' \\ \vdots & \ddots & \vdots \\ \int_{x_0}^{x_1} |x_{c_n} - x'| dS' & \cdots & \int_{x_{n-1}}^{x_n} |x_{c_n} - x'| dS' \end{bmatrix} \begin{bmatrix} \sigma_{n1} \\ \vdots \\ \sigma_{nn} \end{bmatrix} = \begin{bmatrix} \Psi(x_{c_1}) \\ \vdots \\ \Psi(x_{c_n}) \end{bmatrix}$$

One row for each collocation point

# 1st Kind Example

## 1-D Reminder

### Numerical Results



## 2nd Kind Example

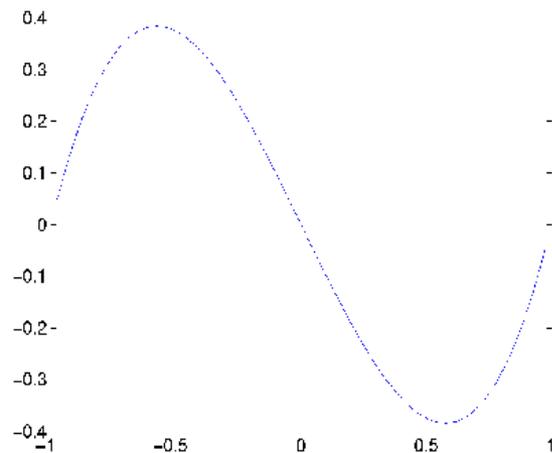
### Second Kind Equation

## 1-D Reminder

$$\Psi(x) = \sigma(x) + \int_{-1}^1 |x - x'| \sigma(x') dS' \quad x \in [-1, 1]$$

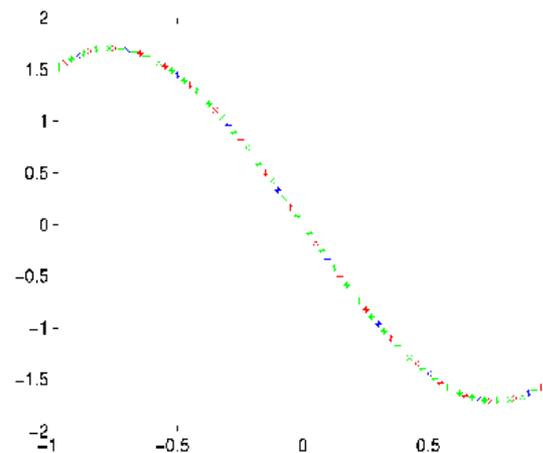
The potential is given

$$\Psi(x) = x^3 - x$$



The density must be computed

$\sigma(x)$  is unknown



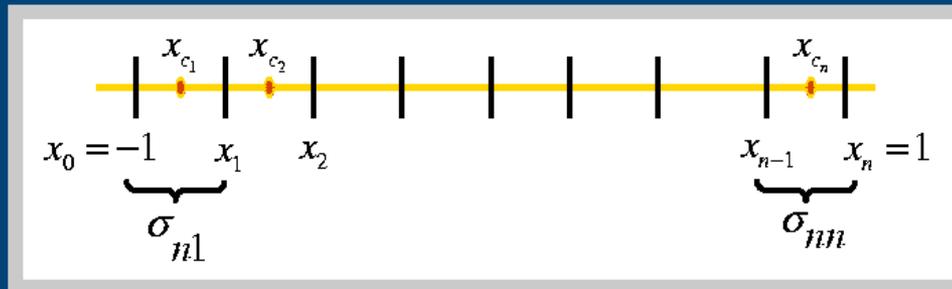
## 2nd Kind Example

### 1-D Reminder

Discretization

$$\Psi(x) = \sigma(x) + \int_{-1}^1 |x - x'| \sigma(x') dS' \quad x \in [-1, 1]$$

### Centroid Collocated Piecewise Constant Scheme



$$\Psi(x_{c_i}) = \sigma_{ni} + \sum_{j=1}^n \sigma_{nj} \int_{x_{j-1}}^{x_j} |x_{c_i} - x'| dS'$$

## 2nd Kind Example

### 1-D Reminder

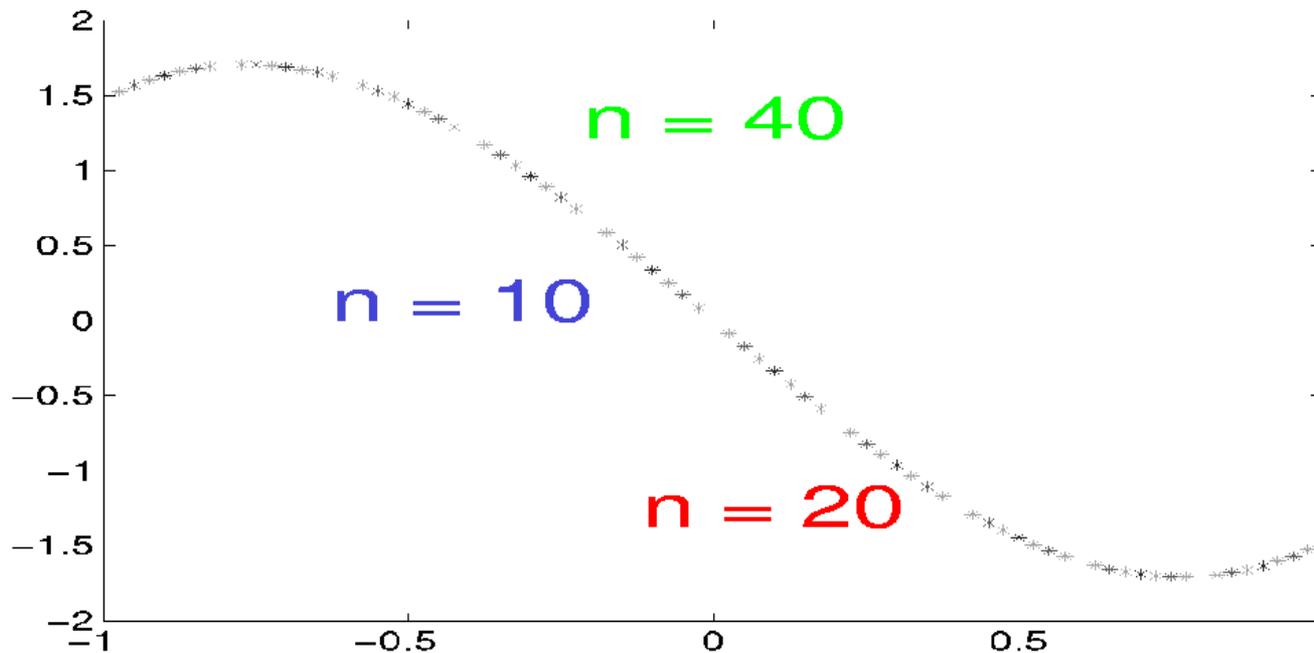
Matrix

$$\begin{bmatrix} 1 + \int_{x_0}^{x_1} |x_{c_1} - x'| dS' & \cdots & \int_{x_{n-1}}^{x_n} |x_{c_1} - x'| dS' \\ \vdots & \ddots & \vdots \\ \int_{x_0}^{x_1} |x_{c_n} - x'| dS' & \cdots & 1 + \int_{x_{n-1}}^{x_n} |x_{c_n} - x'| dS' \end{bmatrix} \begin{bmatrix} \sigma_{n1} \\ \vdots \\ \sigma_{nn} \end{bmatrix} = \begin{bmatrix} \Psi(x_{c_1}) \\ \vdots \\ \Psi(x_{c_n}) \end{bmatrix}$$

## 2nd Kind Example

### 1-D Reminder

Numerical Results



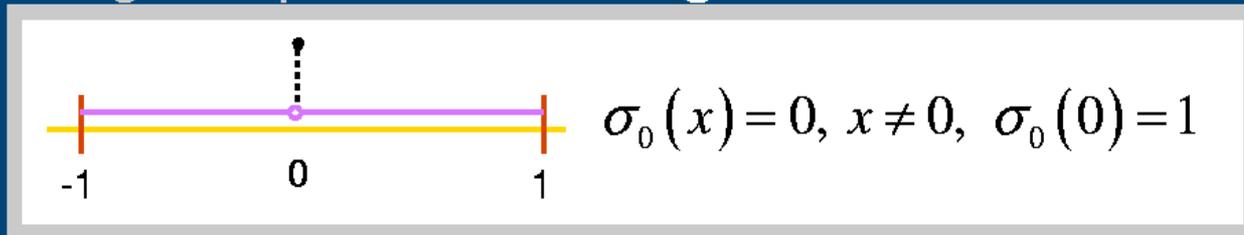
**Answers Are Improving!!!**

## 1-D Reminder

Denote the integral operator as  $K$

$$K\sigma \equiv \int_{-1}^1 |x - x'| \sigma(x') dS' \Rightarrow K\sigma = \Psi$$

The integral operator is **singular** :  $K$  has a null space



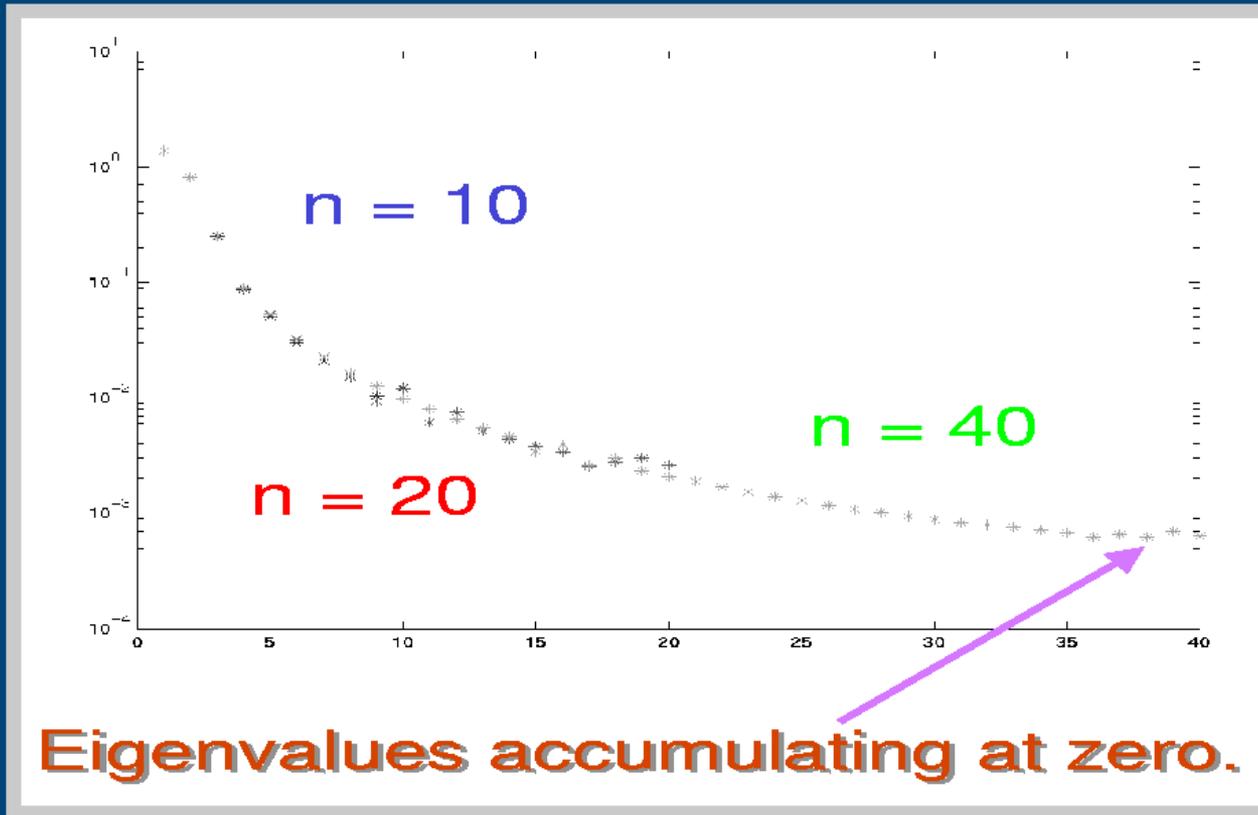
$$K\sigma_0 = \int_{-1}^1 |x - x'| \sigma_0(x') dS' = 0$$

If  $K\sigma^a = \Psi$  then  $K(\sigma^a + \sigma_0) = \Psi$

# 1st Kind Difficulty

## Numerical Results

# 1-D Reminder

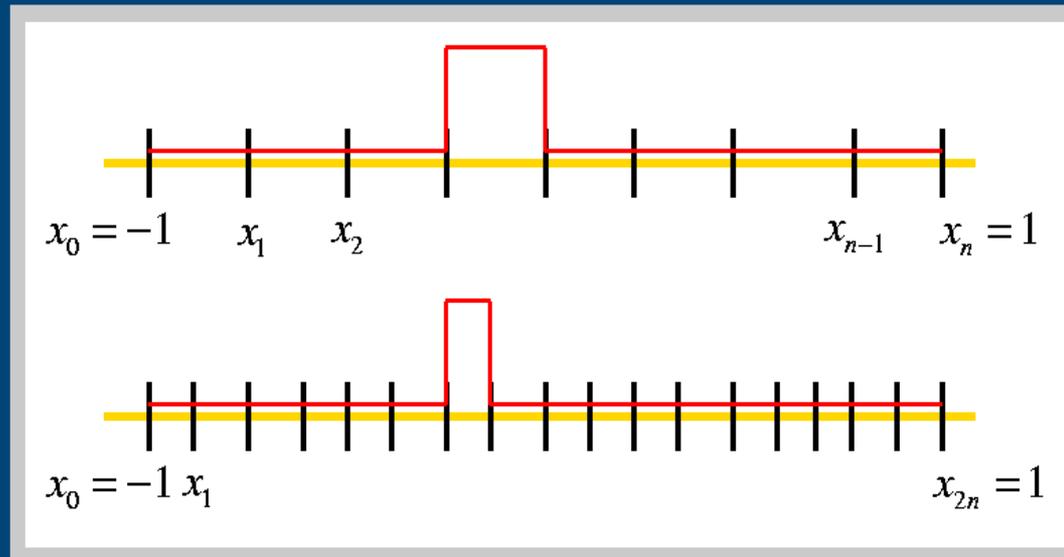


## 1st Kind Difficulty

### Eigenvalues

## 1-D Reminder

As the discretization is refined,  $\sigma_0(x)$  becomes better approximated



As the discretization is refined,  $K$ 's null space can be more accurately represented.

## 1-D Reminder

Second Kind equation

$$(I+K)\sigma \equiv \sigma(x) + \int_{-1}^1 |x-x'| \sigma(x') dS' \Rightarrow (I+K)\sigma = \Psi$$

$$(I+K)(\sigma_0 + \sigma) \neq (I+K)\sigma$$

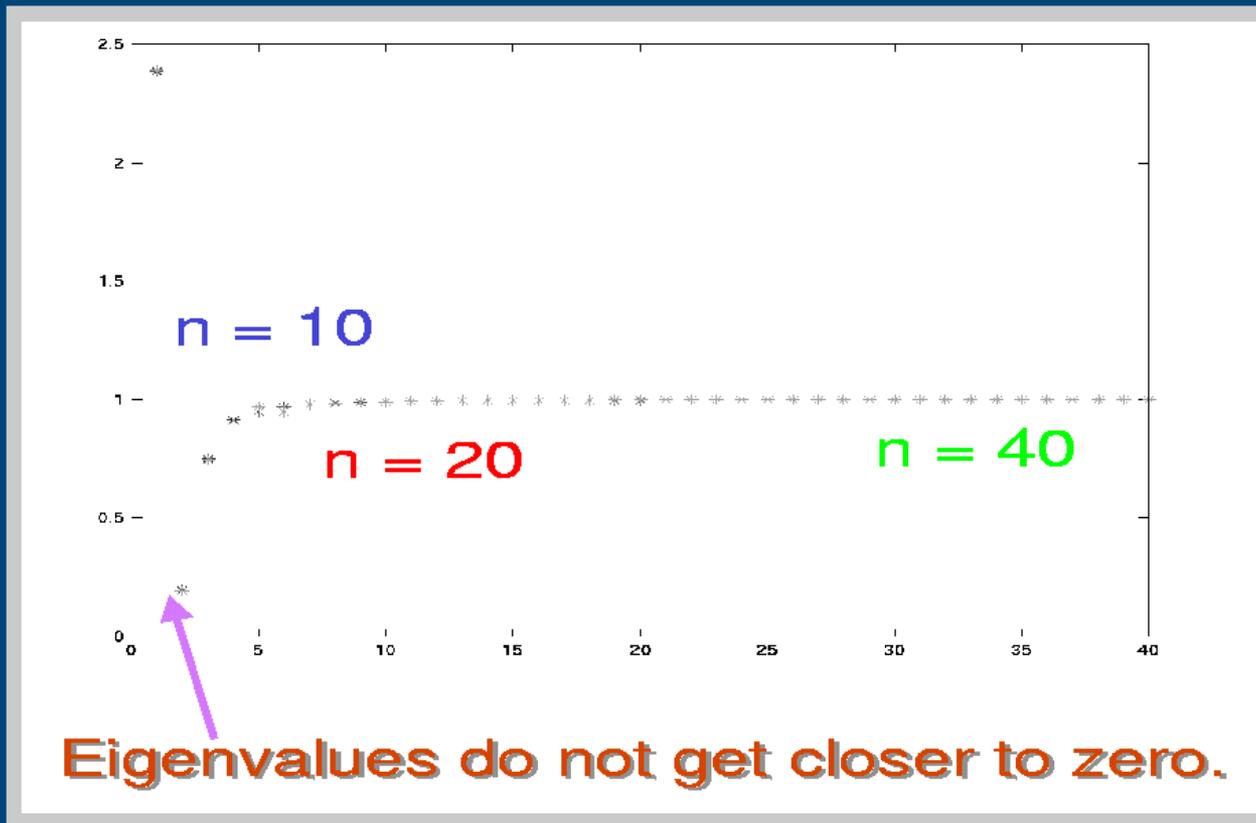
$$(I+K) \left[ \begin{array}{c} \text{Graph 1} \\ \text{Graph 2} \end{array} + \begin{array}{c} \text{Graph 3} \\ \text{Graph 4} \end{array} \right] = \begin{array}{c} \text{Graph 5} \\ \text{Graph 6} \end{array} \neq \Psi$$

$\sigma_0(x) = 0, x \neq 0, \sigma_0(0) = 1$

2nd Kind

Numerical Results

# 1-D Reminder



## 2nd Kind Theorem

### 1-D Reminder

Given  $(I + K)\sigma = \Psi$  and  $\|(I + K)^{-1}\| < C$   
(Equation uniquely solvable)

$$(I + K_n)\sigma_n = \Psi_n$$

(Discrete Equivalent)

### Consistency:

If  $\lim_{n \rightarrow \infty} \max_{\|\sigma_{smooth}\|=1} \|(K - K_n)\sigma\| \rightarrow 0$   
and  $\lim_{n \rightarrow \infty} \|\Psi - \Psi_n\| \rightarrow 0$

### Then

$$\lim_{n \rightarrow \infty} \|\sigma - \sigma_n\| \rightarrow 0$$

## 2nd Kind Theorem

### 1-D Reminder

#### Theorem Meaning

Final result

$$\lim_{n \rightarrow \infty} \|(\sigma_n - \sigma)\| \leq C \lim_{n \rightarrow \infty} \|(K - K_n)\sigma\| = 0$$

What does this mean?

The discretization convergence of a second kind integral equation solver depends on how well the integral is approximated.

## 3-D Laplace

Dirichlet Problem

$$u_{\Gamma}(\vec{x}) = \int_{\Gamma} \frac{1}{\|\vec{x} - \vec{x}'\|} \sigma(\vec{x}') d\Gamma' \quad \vec{x} \in \Gamma$$

Neumann Problem

$$\frac{\partial u_{\Gamma}(\vec{x})}{\partial n_{\vec{x}}} = -2\pi\sigma(\vec{x}') + \int_{\Gamma}^c \frac{\partial}{\partial n_{\vec{x}}} \frac{1}{\|\vec{x} - \vec{x}'\|} \sigma(\vec{x}') d\Gamma'$$

## Interior Examples

### Cauchy Principle Value

## 3-D Laplace

If  $f(\mathbf{y})$  is singular at  $\mathbf{y} = \mathbf{x}_0$ , the Cauchy principle value integral is

$$\int_{\Gamma}^C f(\vec{\mathbf{y}}) d\Gamma \equiv \lim_{\epsilon \rightarrow 0} \int_{|\mathbf{y} - \mathbf{x}_0| \geq \epsilon} f(\vec{\mathbf{y}}) d\Gamma$$

when the limit exists.

If  $\Gamma$  is a flat 2-D surface in 3-D

$$\int_{\Gamma}^C \frac{\partial}{\partial n_{\vec{\mathbf{x}}}} \frac{1}{\|\vec{\mathbf{x}} - \vec{\mathbf{x}}'\|} d\Gamma' = 0 \quad \mathbf{x} \in \Gamma.$$

Define

$$\Psi \equiv \frac{-1}{2\pi} \frac{\partial u_{\Gamma}(\vec{x})}{\partial n_{\vec{x}}}$$

$$K \equiv -\frac{1}{2\pi} \int_{\Gamma}^C \frac{\partial}{\partial n_{\vec{x}}} \frac{1}{\|\vec{x} - \vec{x}'\|} \sigma(\vec{x}') d\Gamma'$$

then the Neumann problem becomes

$$(I + K)\sigma = \Psi$$

Main assumption of second kind theory:

$$(I + K)^{-1}$$

is bounded.

Is  $(I + K)^{-1}$  bounded for the Neumann Problem?

## Linear Algebra

Given  $Ax = b$ ,  $A \in \mathbb{R}^{n \times n}$ ,  $x, b \in \mathbb{R}^n$

$A^{-1}$  exists and is bounded iff

$Ay = 0$  implies  $y = 0$  (no null space)

If  $Ay = 0$  for  $y \neq 0$  then either

$Ax = b$  has an infinite # of solutions

$Ax = b$  then  $A(x + \alpha y) = b$

OR

$Ax = b$  does not have a solution

$b$  is not in column space of  $A$

## 3-D Laplace

## Null Space

Consider  $\tilde{\sigma}$  defined by

$$u_{\Gamma}(\vec{x}) = 1 = \int_{\Gamma} \frac{1}{\|\vec{x} - \vec{x}'\|} \tilde{\sigma}(\vec{x}') d\Gamma' \quad \vec{x} \in \Gamma$$

Then

$$\frac{\partial u_{\Gamma}(\vec{x})}{\partial n_{\vec{x}}} = 0 = -2\pi \tilde{\sigma}(\vec{x}') + \int_{\Gamma} \frac{\partial}{\partial n_{\vec{x}}} \frac{1}{\|\vec{x} - \vec{x}'\|} \tilde{\sigma}(\vec{x}') d\Gamma'$$

$\tilde{\sigma}$  is in the Null space of  $I + K$

$(I + K)^{-1}$  is not bounded!!

## 3-D Laplace

For  $I + K$  either

$(I + K)\sigma = \Psi$  has an infinite # of solutions

OR

$(I + K)\sigma = \Psi$  has no solution

For a solution to exist

$$\int_{\Gamma} \frac{\partial u_{\Gamma}(\vec{x})}{\partial n_{\vec{x}}} d\Gamma = 0$$

## Interior Neumann

# 3-D Laplace

## General Theorem

The 2nd Kind Integral equation has a finite-dimensional Null Space (typically rank one).

## Add a point constraint

Fix  $u$  at some point

## Force $\sigma$ orthogonal to null space

Need the null space

May need to solve 1st kind equation

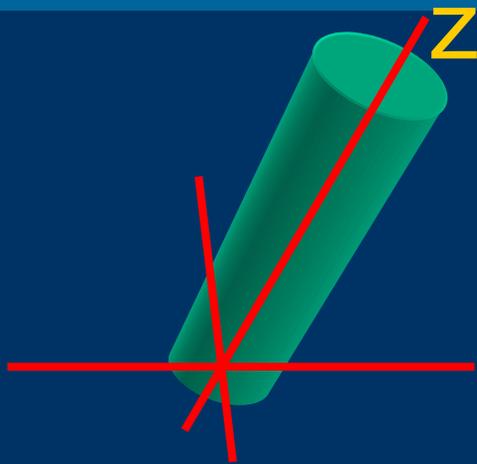
## Use SVD to solve singular system

Can be computationally expensive

# 3-D Laplace's Equation

## First Kind Issues

The singular Kernel Saves the day



### Spike Function=1 on a disk

$$\sigma_0 = 0 \quad \sqrt{x^2 + y^2} > R$$

$$\sigma_0 = 1 \quad \sqrt{x^2 + y^2} \leq R$$

Singular Kernel Case  $\int_{\text{disk}} \frac{1}{\|x_{c_i} - x'\|} \sigma_0(x') dS' = \int_0^R \int_0^{2\pi} \frac{1}{r} r dr d\theta = 2\pi R$

Smooth Kernel Case  $\int_{\text{disk}} 1 \sigma_0(x') dS' = \pi R^2$

Smooth kernel  $\rightarrow 0$  faster as  $R \rightarrow 0$ , more singular

# 3-D Laplace's Equation

## Convergence Analysis

Quick review of FEM  
Convergence for Laplace

Partial Differential Equation form

$$\nabla^2 u = f \quad \text{in } \Omega \quad \Omega \text{ is the volume domain}$$

$$u = 0 \quad \text{on } \Gamma \quad \Gamma \text{ is the problem surface}$$

“Nearly” Equivalent weak form

$$\underbrace{\int_{\Omega} \nabla u \nabla v \, dx}_{a(u,v)} = \underbrace{\int_{\Omega} f v \, dx}_{l(v)} \quad \text{for all } v \in H^1(\Omega)$$

Introduced an abstract notation for the equation  $u$  must satisfy

$$a(u, v) = l(v) \quad \text{for all } v \in H^1(\Omega)$$

# 3-D Laplace's Equation

## Convergence Analysis

### Quick review of FEM Convergence for Laplace

Introduce an approximate solution  $u^n = \sum_{i=1}^n \alpha_i \varphi_i$

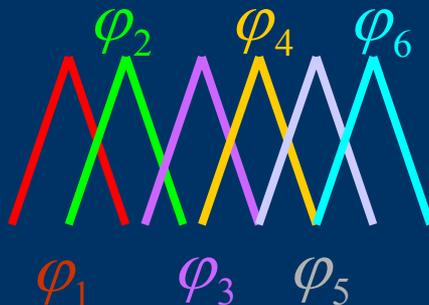
$\Rightarrow u^n$  is a weighted sum of basis functions

The basis functions define a space

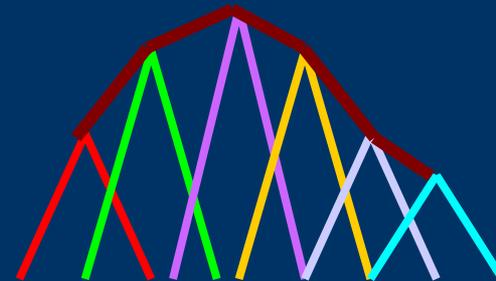
$$X_n = \left\{ v \in X_n \mid v = \sum_{i=1}^n \beta_i \varphi_i \text{ for some } \beta_i \text{'s} \right\}$$

### Example

“Hat” basis functions



Piecewise linear Space



# 3-D Laplace's Equation

## Convergence Analysis

Quick review of FEM  
Convergence for Laplace

### Key Idea

$a(u, u)$  defines a norm on  $H_0^1(\Omega)$      $a(u, u) \equiv \|u\|^2$

U is restricted to be 0 at 0 and 1!!

Using the norm properties, it is possible to show

If  $a(u^n, \varphi_i) = l(\varphi_i)$  for all  $\varphi_i \in \{\varphi_1, \varphi_2, \dots, \varphi_n\}$

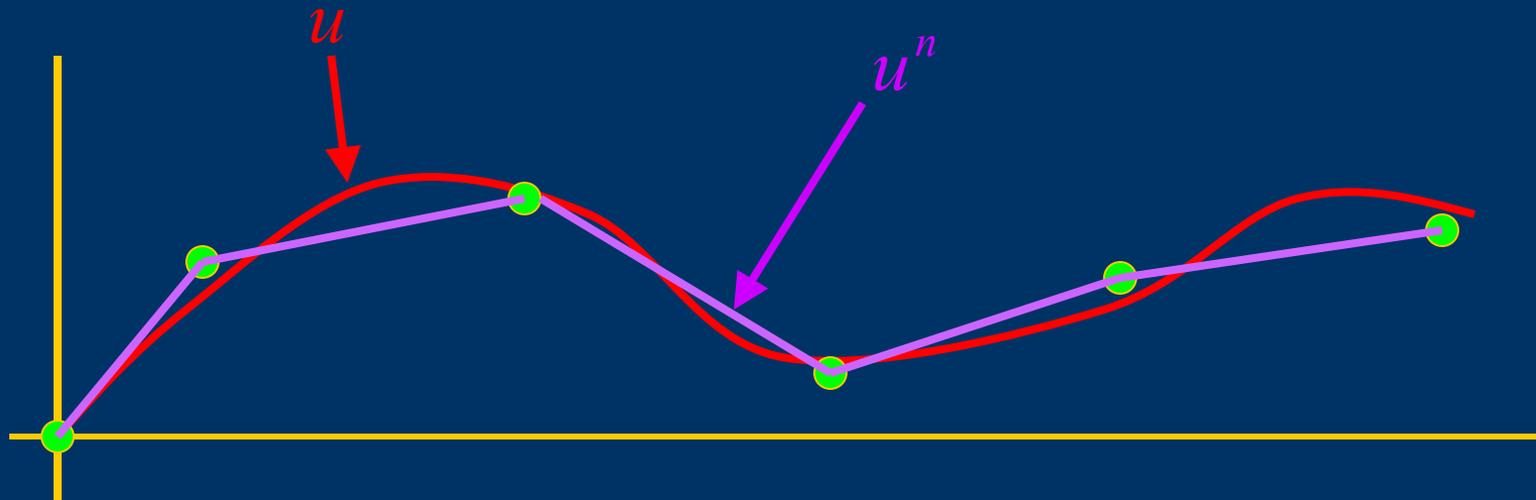
Then  $\underbrace{\|u - u^n\|}_{\text{Solution Error}} = \min_{w^n \in X_n} \underbrace{\|u - w^n\|}_{\text{Projection Error}}$

# 3-D Laplace's Equation

## Convergence Analysis

Quick review of FEM  
Convergence for Laplace

The question is only



How well can you fit  $u$  with a member of  $X_n$

But you must measure the error in the  $\| \cdot \|$  norm

For piecewise linear: 
$$\underbrace{\|u - u^n\|}_{\text{error}} \leq \|u - \Pi_n^a u\| = O\left(\frac{1}{n}\right)$$

# 3-D Laplace's Equation

## Convergence Analysis

Applying FEM approach to first kind integral equations

“Weak” Form for the integral equation

$$\underbrace{\iint_{\Gamma} v(x) \frac{1}{\|x-x'\|} \sigma(x') dS' dS}_{a(\sigma, v)} = \underbrace{\int_{\Gamma} v(x) \Psi(x) dS}_{l(v)} \quad \text{for all } v \in \bar{H}(\Gamma)$$

The difficulty is defining  $\bar{H}(\Gamma)$  with right properties

Must exclude  $\sigma(x)$ 's where  $\int \frac{1}{\|x-x'\|} \sigma(x') dS' = 0$

$\bar{H}(\Gamma)$  is a fractional Sobolev Space

We won't say more about this

# 3-D Laplace's Equation

## Convergence Analysis

Applying FEM approach to first kind integral equations

### Use FEM key Idea

$a(\sigma, \sigma)$  defines a norm on  $\bar{H}(\Gamma)$   $a(\sigma, \sigma) = \|\|\sigma\|\|$

$$\sigma^n = \sum_{i=1}^n \alpha_i \underbrace{\varphi_i(x)}_{\text{Basis Functions}} \quad X_n = \left\{ v \in X_n \mid v = \sum_{i=1}^n \beta_i \varphi_i \text{ for some } \beta_i\text{'s} \right\}$$

Using the norm properties, it is possible to show

*If*  $a(\sigma^n, \varphi_i) = l(\varphi_i)$  **for all**  $\varphi_i \in \{\varphi_1, \varphi_2, \dots, \varphi_n\}$

*Then*  $\underbrace{\|\|\sigma - \sigma^n\|\|}_{\text{Solution Error}} = \min_{w^n \in X_n} \underbrace{\|\|\sigma - w^n\|\|}_{\text{Projection Error}}$

# MEMS Performance Depends on Air Damping of Complicated 3-D Structures

Bosch angular rate sensor

ADXL76 accelerometer

TI 3x3 mirror array

Resonator

Lucent micromirror

# Drag In MEMS is Incompressible Stokes

Velocity integral equation for Stokes flow

$$u_j(\vec{x}_o) = -\frac{1}{8\pi\mu_s} \int f_i(\vec{x}) G_{ij}(\vec{x} - \vec{x}_o) ds$$

where

$$G_{ij} = \frac{\delta_{ij}}{R} + \frac{\hat{x}_i \hat{x}_j}{R^3};$$

$$R = |\vec{x}_o - \vec{x}|; \quad \hat{x}_i = x_{oi} - x_i$$

# Null Space of the Stokes Equation

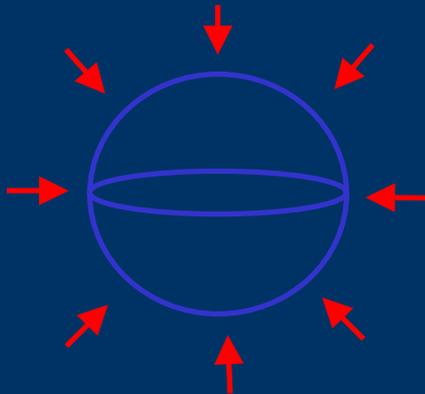
Constant pressure a singular mode, generates zero velocity.

Differential Form of Stokes,  
independent of absolute  
pressure

$$\begin{cases} 0 = -\nabla P + \mu \nabla^2 \vec{u} \\ \nabla \bullet \vec{u} = 0 \end{cases}$$

Integral Form of Stokes,  
constant pressure must not  
change velocity

$$u_j(\vec{x}_o) = -\frac{1}{8\pi\mu} \int_s f_i(\vec{x}) G_{ij}(\vec{x} - \vec{x}_o) ds$$



If  $P = \text{constant}$ ,  $u_i = 0$ ;  $f_i = -P n_i$

$$\Rightarrow \int_s G_{ij}(\vec{x} - \vec{x}_o) n_i(\vec{x}) ds = 0$$

# Null Space of the Singular BEM Operators

- Stokes Integral Operator has a null space
  - The solution is not uniquely defined.
  - A pressure boundary condition is needed.
- Null space must be removed
  - so as to avoid numerical error.

$$F = F^{\text{correct solution}} + \mathbf{XN} + \varepsilon$$

- Two-step method:
  1. Modify GMRES to calculate a null-space-free solution.
  2. Use pressure condition to adjust solution

# Krylov Subspace Iterative methods

## Linear System

Start with  $Ax = b$

Determine the Krylov Subspace  $r^0 = b - Ax^0$

Krylov Subspace  $\equiv \text{span} \{ r^0, Ar^0, \dots, A^k r^0 \}$

Select Solution from the Krylov Subspace

$x^{k+1} = x^0 + y^k, \quad y^k \in \text{span} \{ r^0, Ar^0, \dots, A^k r^0 \}$

GMRES picks a residual-minimizing  $y^k$ .

# Modify Krylov-Subspace Method to Calculate Null-Space-Free Solution

- The discretized Stokes equation  $GF = U$
- The Krylov subspace is

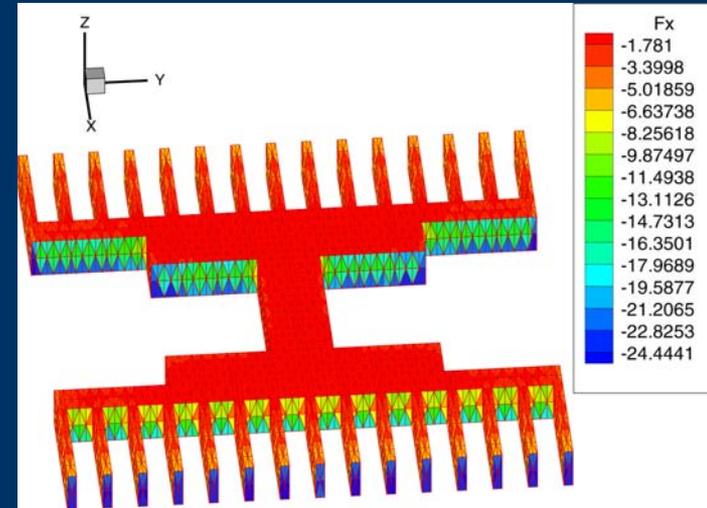
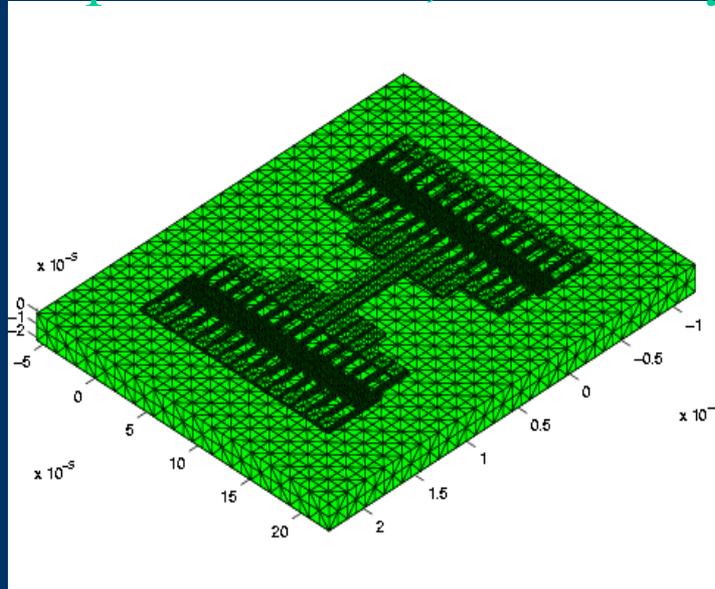
$$\mathcal{K} = \text{span} \{U, GU, G^2U, G^3U, G^4U, \dots\}$$

- If  $\mathcal{K} \perp \text{Null}(G)$  then  $F = F^\perp \perp \text{Null}(G)$

Remove  $\text{Null}(G)$  from every Krylov subspace vector

# FastStokes Simulation Result

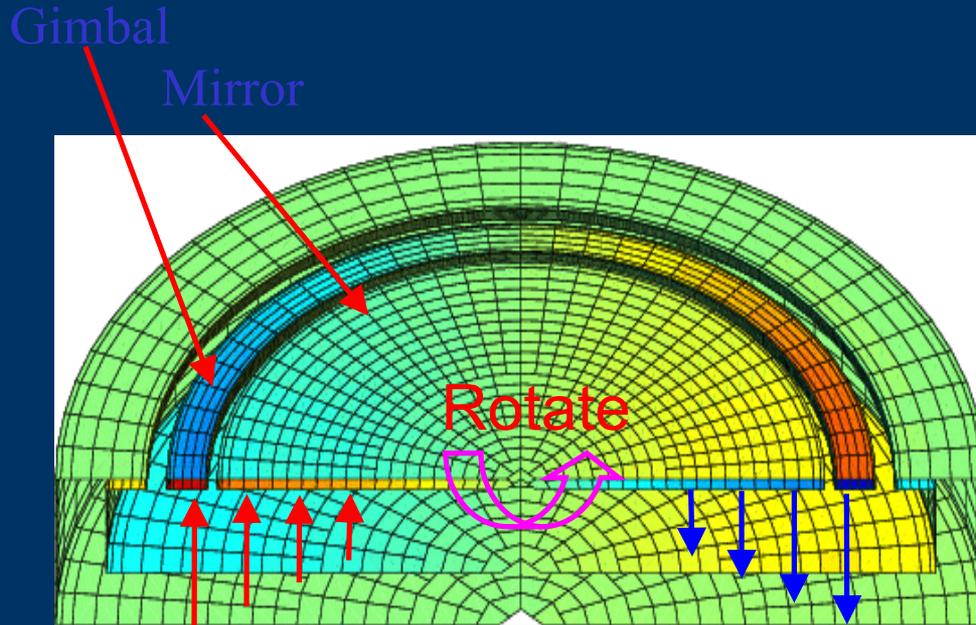
In-plane motion, 3-D steady incompressible Stokes, 16k panels



	Drag Force (nN)					Q
	Total	Bottom	Top	Inter-finger	End and others	
Couette Model	123.7	108.9		14.8		50.1
1-D Stokes	137.1	108.9	13.5	14.8		45.20
FastStokes	223.7	123.0 (55%)	26.8 (12%)	73.8 (33%)		27.7
Measurement						27

Computation finished in 10 minutes

# Micromirror Q-factor



	Mode	Q		Error (%)
		Simulated	Measured	
Mirror 1	Mirror+Gimbal	2.36	2.31	2.16
	Mirror	3.14	3.45	8.99
Mirror 2	Mirror+Gimbal	4.69	4.27	9.84
	Mirror	10.16	10.63	4.42

# Summary

Reminder about 2<sup>nd</sup> Kind theory

Convergence Theory

Fredholm Alternative for 2<sup>nd</sup> Kind

Finite Dimensional Null Space

First Kind Convergence Theory, sort of

Connection to the FEM results

MEMS Drag Example