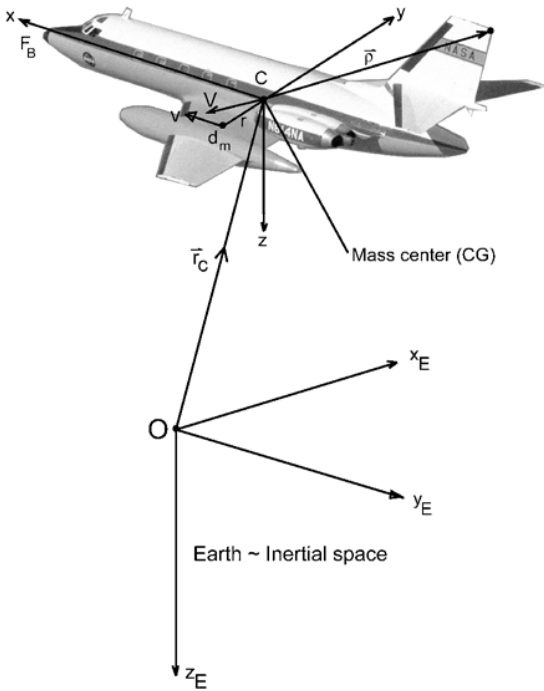


AEROSPACE DYNAMICS

EXAMPLE : GIVE ACCELERATION OF THE TIP OF THE RUDDER ON THIS AIRCRAFT



- LOOKING FOR ABSOLUTE ACCELERATION WITH RESPECT TO THE INERTIAL FRAME (EARTH IN THIS CASE)
- DEFINE A BUNCH OF POINTS AND VECTORS OF INTEREST
 - \vec{r}_C - LOCATION OF A/C COM WRT THE ORIGIN
 - \vec{p} - LOCATION OF RUDDER TIP WRT A/C COM

- ATTACH A FRAME TO THE AIRCRAFT (x, y, z) - CALLED A "BODY FRAME"
- ASSUME THAT AIRCRAFT MASS CENTER HAS VELOCITY \vec{V}_{cm} AND ANGULAR VELOCITY OF THE VEHICLE WRT INERTIAL SPACE IS $\vec{\omega}$

NOTE THAT $\vec{r}_r = \vec{r}_{cm} + \vec{p}$
 WANT TO FIND $\ddot{\vec{r}}_r^I$

$(\dot{\cdot})^I$ - MEANS DERIVATIVE WRT TIME AS SEEN IN INERTIAL FRAME

- TO COMPUTE $\ddot{\vec{r}}_r^I$ (INERTIAL ACCELERATION) WE WILL START BY FIRST COMPUTING $\dot{\vec{r}}_r^I$
- KEY POINT: OBSERVER ON THE AIRCRAFT CAN TELL US WHAT THE RUDDER IS DOING WITH RESPECT TO THE A/C COM
 - BUT WE NEED TO ACCOUNT FOR THE AIRCRAFT MOTIONS AS WELL.
- KNOW THAT: $\dot{\vec{r}}_r^I = \dot{\vec{r}}_{cm}^I + \dot{\vec{p}}^I$

QUESTION - HOW DO WE RELATE $\dot{\vec{p}}^I$ TO THE CHANGES THAT WE CAN SEE IN THE AIRCRAFT?

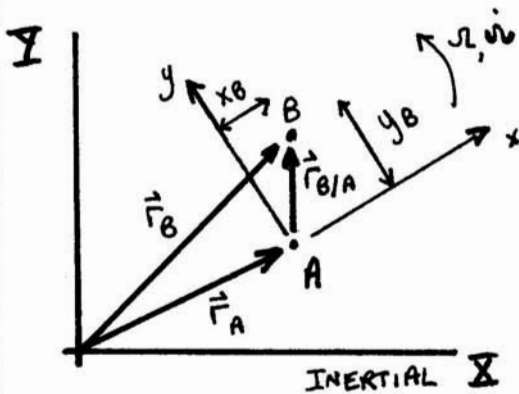
- CHANGES AS SEEN BY AN OBSERVER ARE DENOTED AS $\dot{\vec{p}}^B$

- KEY POINT: MUST BE CAREFUL THAT THE DIFFERENTIATION IS CARRIED OUT IN THE PROPER REFERENCE FRAME.

- SOLUTION IS TO USE THE "TRANSPORT THEOREM" OR "CORIOLIS LAW"

$$\Rightarrow \dot{\vec{r}}^I = \dot{\vec{r}}^B + \vec{\omega} \times \vec{r}$$

- WHERE DOES THIS EXPRESSION COME FROM?
 - CONSIDER SIMPLER 2D CASE
 - 2 POINTS "A", "B" WITH A FIXED AND B FREE TO ROTATE AROUND A



$$\Rightarrow \vec{r}_B = \vec{r}_A + \vec{r}_{B/A}$$

- AT THIS INSTANT, POINT A HAS ZERO VELOCITY AND ANGULAR VELOCITY / ACCELERATION ABOUT Z-AXIS OF $\vec{\omega}, \vec{\alpha}$

- FRAMES: X, Y INERTIAL, x, y AT "A" AND ROTATING.

- OBJECTIVE IS TO FIND

$$\vec{v}_B = \dot{\vec{r}}_B^I = \dot{\vec{r}}_A^I + \dot{\vec{r}}_{B/A}^I \equiv \frac{d^I}{dt} (\vec{r}_{B/A})$$

- $\vec{r}_{B/A} = x_B \vec{i} + y_B \vec{j}$

⇒ "PROJECTION" OR REPRESENTATION OF VECTOR $\vec{r}_{B/A}$ IN TERMS OF THE CURRENT DIRECTIONS OF THE FRAME ATTACHED TO "A"

- TO COMPUTE THE DERIVATIVE $\frac{d^I}{dt}(\vec{r}_{B/A})$ WE MUST ACCOUNT FOR CHANGES IN BOTH

- x_B, y_B

- \vec{i}, \vec{j}

- $$\frac{d^I}{dt}(\vec{r}_{B/A}) = \underbrace{\frac{dx_B}{dt} \vec{i} + \frac{dy_B}{dt} \vec{j}}_{\text{TIME RATE OF CHANGE WITH FRAME FIXED.}} + \underbrace{x_B \frac{d\vec{i}}{dt} + y_B \frac{d\vec{j}}{dt}}_{\text{INSTANTANEOUS TIME RATE OF CHANGE OF UNIT VECTORS THAT DEFINE FRAME "A" AS MEASURED BY INERTIAL OBSERVER}}$$

TIME RATE OF CHANGE WITH FRAME FIXED.
- SAME FOR BOTH OBSERVERS

⇒ SAME AS VELOCITY OF POINT B AS MEASURED BY AN OBSERVER IN FRAME A

$$\vec{v}_{B/A}^A$$

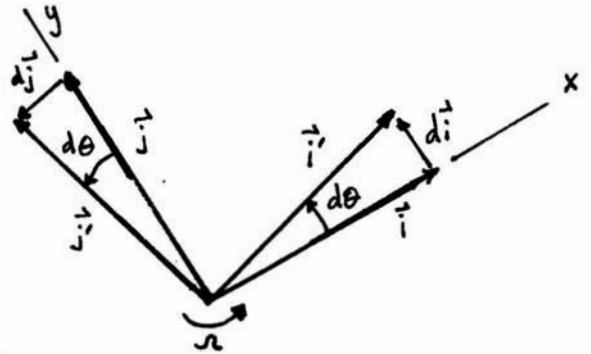
INSTANTANEOUS TIME RATE OF CHANGE OF UNIT VECTORS THAT DEFINE FRAME "A" AS MEASURED BY INERTIAL OBSERVER

- OK SO FAR, BUT HOW DO THESE UNIT VECTORS CHANGE WITH TIME?

- FRAME A KNOWN TO BE ROTATING WITH RATE $\vec{\omega} = \omega \vec{k}$

- DUE TO THE ROTATION

$$\begin{aligned}\vec{i} &\rightarrow \vec{i}' = \vec{i} + d\vec{i} \\ \vec{j} &\rightarrow \vec{j}' = \vec{j} + d\vec{j}\end{aligned}$$



- NOTE: - $d\vec{i}$ AND $d\vec{j}$ ARE DUE ONLY TO THE INSTANTANEOUS ROTATION $d\theta$ ABOUT THE Z-AXIS,
 - ASSUMED TO BE A VERY SMALL ROTATION OVER A SHORT TIME PERIOD.

- CAN WRITE THAT $|d\vec{i}| = 1 |d\theta|$ ARC LENGTH
- DIRECTION OF $d\vec{i}$ IS IN THE $+\vec{j}$ DIRECTION WHICH IS TANGENT TO PATH FOLLOWED BY TIP OF \vec{i} .

$$\Rightarrow d\vec{i} = \vec{j} d\theta \quad \text{so} \quad \frac{d\vec{i}}{dt} = \frac{d\theta}{dt} \vec{j}$$

WHAT ABOUT $d\vec{j}$?

WHAT IS $\frac{d\theta}{dt}$?

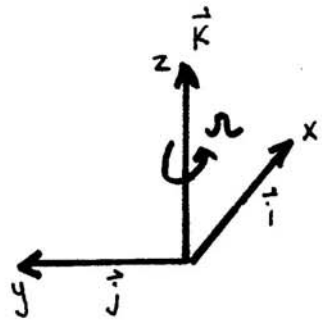
• NOTE $\frac{d\vec{e}}{dt} = \vec{\omega}$ WHY?

AND $\frac{d\vec{i}}{dt} = \vec{\omega} \times \vec{j}$; $\frac{d\vec{j}}{dt} = -\vec{\omega} \times \vec{i}$

⇒ MORE COMPACT FORM IS :

$$\frac{d\vec{i}}{dt} = \vec{\omega} \times \vec{i}$$

$$\frac{d\vec{j}}{dt} = \vec{\omega} \times \vec{j}$$



• SO CAN WRITE

$$\begin{aligned} x_B \frac{d\vec{i}}{dt} + y_B \frac{d\vec{j}}{dt} &= \vec{\omega} \times x_B \vec{i} + \vec{\omega} \times y_B \vec{j} \\ &= \vec{\omega} \times (x_B \vec{i} + y_B \vec{j}) = \vec{\omega} \times \vec{r}_{B/A} \end{aligned}$$

• SUMMARY :

$$\vec{v}_B = \dot{\vec{r}}_B^I = \dot{\vec{r}}_{B/A}^A + \vec{\omega} \times \vec{r}_{B/A} = \dot{\vec{r}}_{B/A}^I$$

- SAME AS OUR TRANSPORT THEOREM WITH

$$\vec{r}_{B/A} \rightsquigarrow \vec{r}$$

- SO WE CAN WRITE

$$\dot{\vec{p}}^I = \dot{\vec{p}}^B + \vec{\omega} \times \vec{p}$$

$$\Rightarrow \dot{\vec{\Gamma}}_r^I = \dot{\vec{\Gamma}}_{cm}^I + \dot{\vec{p}}^B + \vec{\omega} \times \vec{p}$$

- TO COMPUTE THE ACCELERATION, MUST TAKE THE SECOND DERIVATIVE:

$$\ddot{\vec{\Gamma}}_r^I = \ddot{\vec{\Gamma}}_{cm}^I + \frac{d^I}{dt}(\dot{\vec{p}}^B) + \frac{d^I}{dt}(\vec{\omega} \times \vec{p})$$

- \Rightarrow APPLY TRANSPORT THEOREM IN EACH CASE:

$$\frac{d^I}{dt}(\dot{\vec{p}}^B) = \ddot{\vec{p}}^B + \vec{\omega} \times \dot{\vec{p}}^B$$

$$\begin{aligned} \frac{d^I}{dt}(\vec{\omega} \times \vec{p}) &= \dot{\vec{\omega}}^I \times \vec{p} + \vec{\omega} \times \frac{d^I}{dt}\vec{p} \\ &= \dot{\vec{\omega}}^I \times \vec{p} + \vec{\omega} \times (\dot{\vec{p}}^B + \vec{\omega} \times \vec{p}) \end{aligned}$$

$$\therefore \ddot{\vec{\Gamma}}_r^I = \ddot{\vec{\Gamma}}_{cm}^I + \ddot{\vec{p}}^B + 2\vec{\omega} \times \dot{\vec{p}}^B + \dot{\vec{\omega}}^I \times \vec{p} + \vec{\omega} \times (\vec{\omega} \times \vec{p})$$

- PROBABLY HAVE SEEN THIS EXPRESSION BEFORE
 - FUNDAMENTAL FORM OF THE RELATIONSHIP BETWEEN ACCELERATIONS AS VIEWED IN FRAMES THAT ARE ROTATING ($\vec{\omega}$) AND ACCELERATING ($\ddot{\vec{\Gamma}}_{cm}^I, \dot{\vec{\omega}}^I$) WRT EACH OTHER.

• INDIVIDUAL COMPONENTS:

- ① $\ddot{\Gamma}_{cm}^I$ - ACCELERATION OF B FRAME WRT I
- ② $\ddot{\vec{r}}^B$ - ACCELERATION OF RUDDER AS SEEN BY OBSERVER IN B AT C.M.
- ③ $2\vec{\omega} \times \dot{\vec{r}}^B$ - CORIOLIS ACCELERATION
- ④ $\dot{\vec{\omega}}^I \times \vec{r}$ - ANGULAR ACCELERATION
- ⑤ $\vec{\omega} \times (\vec{\omega} \times \vec{r})$ - CENTRIPETAL ACCELERATION.

- WILL SPEND TIME ANALYZING THESE IN DETAIL
 - ORDER OF MAGNITUDE?
 - CENTRIPETAL ACCELERATION AT EARTH'S SURFACE?

- KEY IS TO "CORRECTLY" SELECT THE FRAMES AND TO IDENTIFY ALL ANGLES/ ANGULAR RATES BETWEEN THEM.

⇒ THERE ARE FORMAL WAYS (I.E. STANDARD WAYS) OF TRACKING AND DEFINING THESE ANGLES.

- FOCUS OF THIS CLASS WILL BE ON THE METHODOLOGY OF PROBLEM SOLVING.

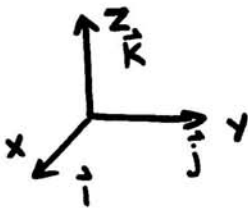
- F A R M

- FRAMES
- ANGLES
- ROTATIONS
- MECHANICS

⇒ TRICK IS TO BE SYSTEMATIC IN YOUR APPROACH TO THE PROBLEMS AND THAT WILL _{HELP} YOU SOLVE THEM FASTER + BETTER.

- ① VECTOR - QUANTITY THAT HAS BOTH A DIRECTION AND A MAGNITUDE. \vec{F}
- INDEP. OF COORDINATE FRAME

- ② COORDINATE FRAME - RIGHT HANDED TRIAD OF UNIT VECTORS (ORTHOGONAL) THAT SPAN 3-SPACE

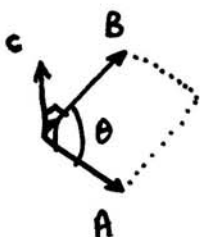


- ③ INERTIAL FRAME - ANY FRAME IN WHICH MOTION CAN BE DESCRIBED BY NEWTON'S LAWS
- IN GENERAL, FIXED RELATIVE TO THE STARS

NOT ACCELERATING OR ROTATING

- OFTEN FIND THAT FRAMES FIXED TO THE EARTH ARE "INERTIAL ENOUGH"
- \Rightarrow FUNCTION OF TIMESCALE + LENGTH OF MOTIONS UNDER CONSIDERATION.

$$\textcircled{A} \vec{C} = \vec{A} \times \vec{B} \quad \Rightarrow \quad |\vec{C}| = |\vec{A}| \cdot |\vec{B}| \sin \theta$$



θ - ANGLE BETWEEN \vec{A} AND \vec{B}

$|\vec{C}|$ = AREA OF PARALLELOGRAM DEFINED BY \vec{A} , \vec{B}

• CROSS PRODUCT $\vec{C} = \vec{A} \times \vec{B}$

$$\vec{C} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ A_1 & A_2 & A_3 \\ B_1 & B_2 & B_3 \end{vmatrix} = \hat{i} \begin{vmatrix} A_2 & A_3 \\ B_2 & B_3 \end{vmatrix} - \hat{j} \begin{vmatrix} A_1 & A_3 \\ B_1 & B_3 \end{vmatrix} + \hat{k} \begin{vmatrix} A_1 & A_2 \\ B_1 & B_2 \end{vmatrix}$$

• CAN SHOW THAT IF REPRESENTATION OF VECTOR $\vec{A} = A_1 \hat{i} + A_2 \hat{j} + A_3 \hat{k}$

→ MATRIX FORM $\begin{bmatrix} A_1 \\ A_2 \\ A_3 \end{bmatrix}$

GIVES THE COMPONENTS IN THE $\hat{i}, \hat{j}, \hat{k}$ FRAME

AND \vec{B} HAS REPRESENTATION $\begin{bmatrix} B_1 \\ B_2 \\ B_2 \end{bmatrix}$

THEN MATRIX REPRESENTATION OF \vec{C} GIVEN

BY

$$\begin{bmatrix} C_1 \\ C_2 \\ C_3 \end{bmatrix} = \begin{bmatrix} 0 & -A_3 & A_2 \\ A_3 & 0 & -A_1 \\ -A_2 & A_1 & 0 \end{bmatrix} \begin{bmatrix} B_1 \\ B_2 \\ B_3 \end{bmatrix} = A^x B$$