

16.50 Homework 10 Solution

a) Calculate the degree of reaction and the flow angles at the stator and rotor exits (β_b, β'_c). Draw the velocity triangle to scale. Also, sketch the blade shapes of the stator and rotor.

$$\Psi = 1.6; \quad \phi = 0.8; \quad T_{t,a} = T_{t,4} = 1800 \text{ K}; \quad \gamma = 1.4; \quad R = 287 \frac{\text{J}}{\text{kg K}}$$

$$R = 1 - \frac{\Psi}{2} = 0.2; \quad \beta_b = \tan^{-1}\left(\frac{\Psi}{\phi}\right) = 63.43^\circ; \quad \beta'_c = \tan^{-1}\left(\frac{1}{\phi}\right) = 51.34^\circ$$

b) Calculate the velocity (V_b) entering the rotor, and the axial velocity component, u . Then, calculate the wheel speed and the total temperature drop in the stage. Finally, calculate the total pressure ratio of the stage, Π_t .

Flow is choked at stator exit, so the Mach number at 'b' is one:

$$T_b = \frac{T_{t,a}}{1 + \frac{\gamma-1}{2} \cdot 1^2} = \frac{1800 \text{ K}}{1.2} = 1500 \text{ K} \rightarrow V_b = \sqrt{\gamma R T_b} = 776 \frac{\text{m}}{\text{s}}$$

$$u = V_b \cos(\beta_b) = 347 \frac{\text{m}}{\text{s}} \rightarrow (\omega r) \frac{u}{\phi} = 434 \frac{\text{m}}{\text{s}}$$

From Euler's Equation:

$$\Delta T_t = \frac{(\omega r)^2 \Psi}{c_p} = \frac{434^2 \cdot 1.6}{1004.5} = 300 \text{ K} \rightarrow \tau_t = \frac{1500 \text{ K}}{1800 \text{ K}} = 0.833$$

$$\eta_{\text{turbine}} = \frac{\text{actual work extracted}}{\text{ideal work extracted}} = \frac{T_{t,4} - T_{t,5}}{T_{t,4} - (T_{t,5})_{\text{ideal}}} = \frac{1 - \tau_t}{1 - \Pi_t^{\frac{\gamma-1}{\gamma}}} \rightarrow \Pi_t = \left(1 - \frac{1 - \tau_t}{\eta_{\text{turbine}}}\right)^{\frac{\gamma}{\gamma-1}} = 0.50$$

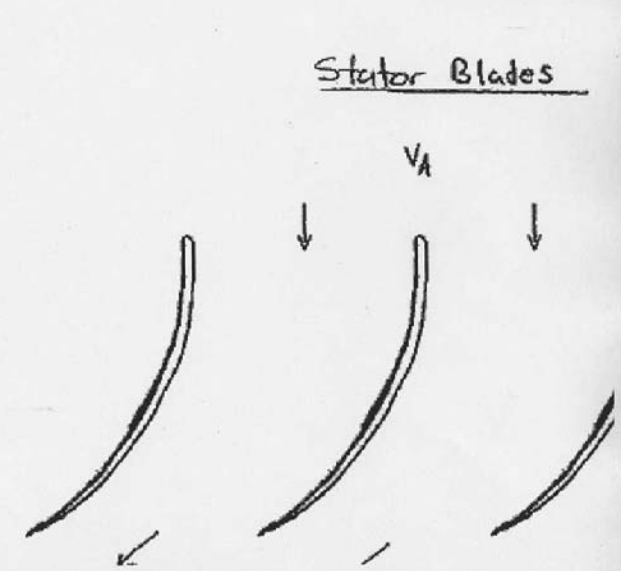
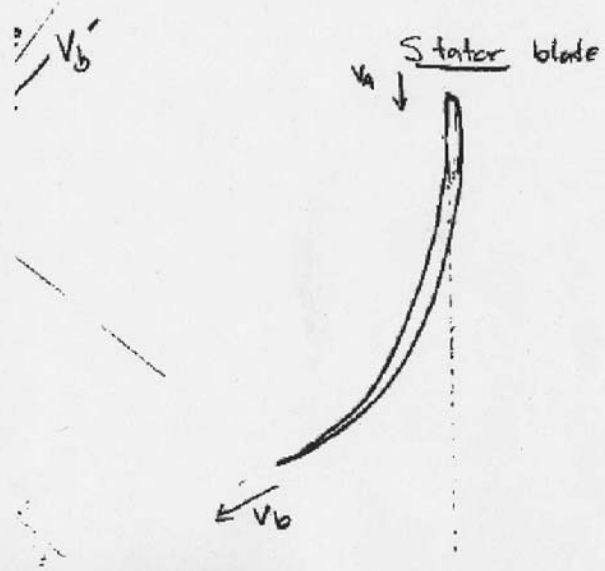
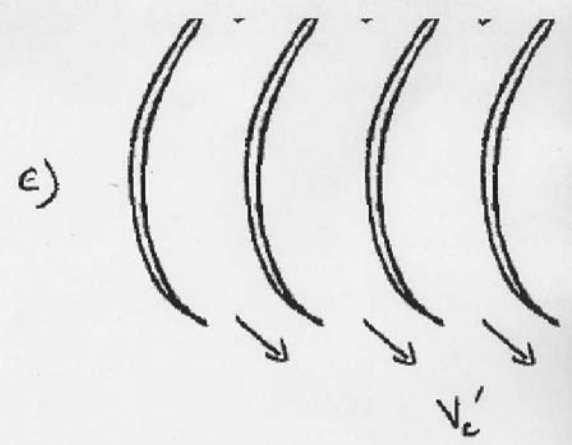
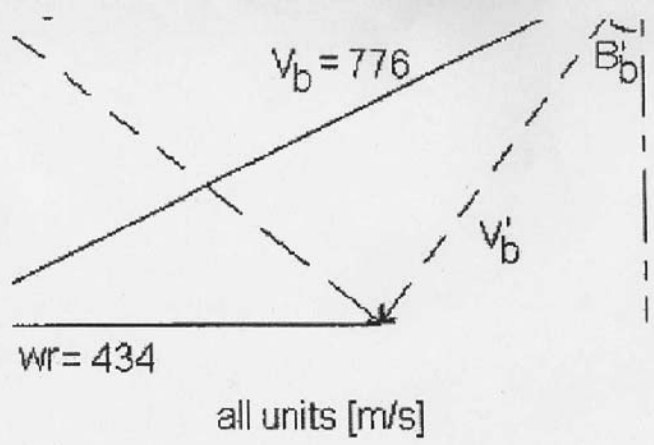
(c) Calculate the axial solidity ratio of the stator and rotor so that the Zweifel coefficient is 0.8. Sketch a few blades each of the stator and rotor, assuming the same axial chord in both cases.

$$\text{Stator: } \left(\frac{c_x}{s}\right)_s = \frac{\sin(2\beta_b) \left|\frac{v_a}{v_b} - 1\right|}{\Psi_z} = 1$$

$$\text{Rotor: } \left(\frac{c_x}{s}\right)_r = \frac{\sin(2\beta'_c) \left|\frac{v'_b}{v'_c} - 1\right|}{\Psi_z}; \quad v'_b = v_b - \omega r = \omega r(\Psi - 1); \quad v'_c = -\omega r; \quad \frac{v'_b}{v'_c} = 1 - \Psi$$

$$\left(\frac{c_x}{s}\right)_r = \frac{\sin(2\beta'_c) |1 - \Psi - 1|}{\Psi_z} = \sin(102.68^\circ) \frac{1.6}{0.8} = 1.951$$

Thus, for equal axial chord lengths, the rotor blades are spaced almost twice as close together as the stator blades.



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