

4.5 > Integral Methods

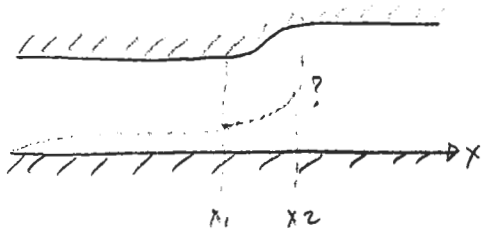
- A > BL behavior example
- B > Sep. behavior
- C > Separation in TSL Context

Reading: Handout paper

A > BL Behavior estimate Example

Goal: Gain insight into how various terms in the 2-egm method drive BL behavior

Problems:



$$\left(\frac{u_{e2}}{u_{e1}}\right) = 0.9$$

• Sudden decrease (10%) in  $u_e$  on a flat plate BL

- a) Will BL separate?
- b) What is the  $\theta$  increase?

Use logarithmic form of mom & K.E eqn

$$\frac{d}{dx}(\ln \theta) = \frac{1}{\theta} \frac{g}{2} - (2+H) \frac{d}{dx}(\ln u_e)$$

$$\frac{d}{dx}(\ln H^*) = \frac{1}{\theta} \left[ \frac{2C_D}{H^*} - \frac{g}{2} \right] + (H-1) \frac{d}{dx}(\ln(u_e))$$

To check for separation we use K.E shape param eqn.

$$\int_{x_1}^{x_2} \left\{ \right\} dx$$

$$\frac{H_2^*}{H_1^*} \approx \exp \left\{ \left[ \frac{2C_D}{H^*} - \frac{g}{2} \right] \frac{1}{\theta_{avg}} (x_2 - x_1) \right\} \cdot \left(\frac{u_{e2}}{u_{e1}}\right)^{(H-1)_{avg}}$$

Examine limits in K-E eqn  $\rightarrow du/dx < 0 \Rightarrow H^*$  getting smaller  
 for sufficiently fast deceleration  $x_2 - x_1 \rightarrow 0$

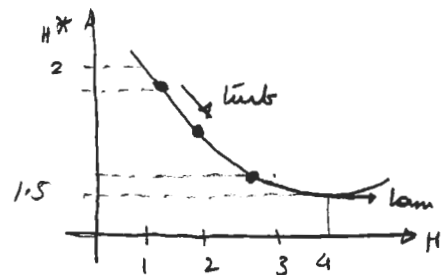
(2)

$$\Rightarrow \exp \left\{ \dots \right\} \rightarrow 1$$

$$\therefore \left( \frac{H_2^*}{H_1^*} \right) \approx (0.9)^{(H-1)_{avg}}$$

For laminar flow

$$H_1 \approx 2.6, H_1^* \approx 1.55$$



$$\text{Turbulent } H_1 \approx 1.4, H_1^* \approx 1.85$$

$$\therefore H_2^* \approx (0.9)^{1.6} H_1^* = 0.84 \times H_1^* = 1.3 \Rightarrow \text{flow will separate below } H^* \approx 1.5 \text{ sep. limit}$$

$$H_2^* = (0.9)^{0.4} H_1^* = 1.78 \Rightarrow \text{far from separation}$$

Estimate  $\theta_2$  for turbulent flow

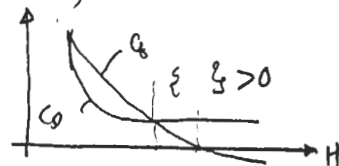
$$\ln \frac{\theta_2}{\theta_1} \approx -(H+2) \ln 0.9$$

$$\Rightarrow \frac{\theta_2}{\theta_1} \approx 1.43 \text{ sudden increase in } \theta$$

If  $\Delta x$  is large,  $\theta_1$  will be additional contribution from  $q$  term

For slower deceleration, the terms that multiply  $\Delta x$  alleviate the effects of the pressure gradient, but add to  $\theta$  increase

$$\left\{ \frac{2C_0}{H^*} - q/2 \right\}$$

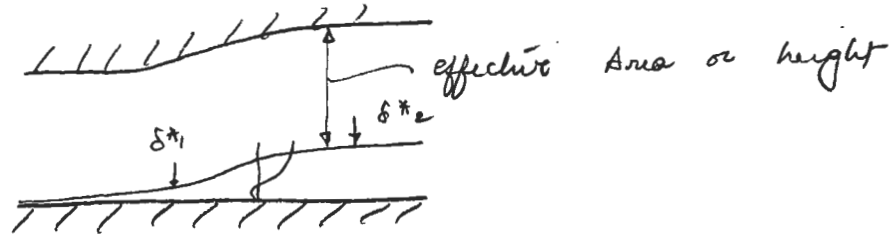


As  $H$  increases  $\left\{ \right\}$  becomes more positive and drive  $H^*$  bigger to alleviate the tendency to separate

Going back to laminar case

$$H^* \approx 1.3$$

which is below the min "permitted" by  $H^*(H)$  correlation function. In reality, the flow will separate and moderate the  $u_e$  decrease via the blockage or displacement effect (next series on IBLT) so that  $H^* \rightarrow$  approach 1.5

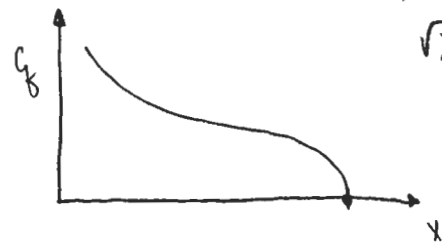


Separation Singularity

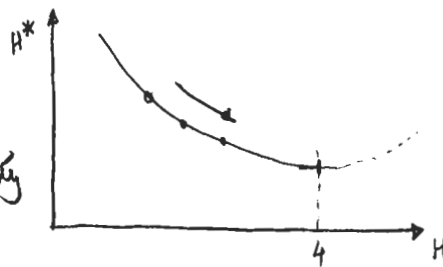
Consider a different view . . .

$$\frac{dH}{dx} = \frac{1}{dH^*/dH} \left\{ \frac{1}{\sigma} \left( \frac{\partial C_D}{\partial H^*} - \frac{q}{\delta/2} \right) + (H-1) \frac{1}{u_e} \frac{du_e}{dx} \right\}$$

Towards separation point with  $u_e(x)$  prescribed



$\sqrt{x}$  singularity



$$H^* \approx 1.5 + K(H-4)^2$$

$$\frac{dH^*}{dH} = 2K(H-4)$$

$$\frac{dH}{dx} = \frac{1}{2K(H-4)} \{ \quad \}$$

$$\Rightarrow \frac{d(H-4)}{dx} = \frac{a}{H-4}$$

$$\frac{1}{2}(H-4) = \sqrt{cx}$$

0.019

As  $H \rightarrow 4$ ,  $\frac{dH^*}{dH} \rightarrow 0$

$\therefore \frac{dH}{dx} \rightarrow \infty$ ,  $\frac{dC_f}{dx}, \frac{dC_D}{dx} \rightarrow \infty$

called "Goldstein singularity". Purely numerical artifact occurs when  $u_e(x)$  is imposed at separation (solution is infinitely sensitive to imposed problem)

We can see that  $\frac{dH}{dx}$  is finite only if

$$\left\{ \frac{2C_0}{H^*} - \frac{g/2}{\theta} \right\} \frac{1}{u_c} + (H-1) \frac{1}{u_c} \frac{du_c}{dx} = 0 \text{ at separation}$$

or  $u_c(x)$  is such that  $\frac{du_c}{dx} \approx -\frac{2C_0}{H^*} \frac{(u_c/\theta)}{(H-1)}$   $\approx$  large

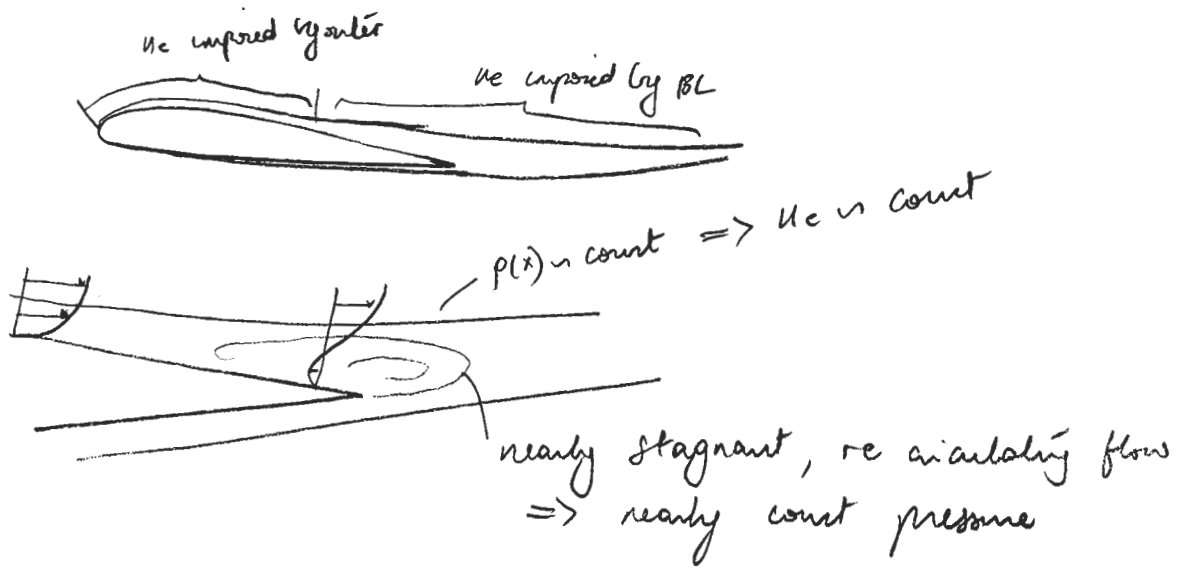
$$(H-1) \frac{\theta}{u_c} \frac{du_c}{dx} = \frac{g/2}{\theta} - \frac{2C_0}{H^*} \text{ at separation}$$

$\Rightarrow$  boundary layer determines  $u_c(x)$  (in channel example or blockage (or  $\delta^*$ ) mechanism. ( $\frac{du_c}{dx}$  is determined by  $g$ )

In other words,

Note - This requires IBLT displacement effect, so that BL can modify  $u_c$  so that  $\frac{du_c}{dx}$  reaches the "admissible" value

$\frac{du_c}{dx}$  is quite small in separated flow regions



# B) Separation in TSL Context

We can deal with limited separation

• TSL assumption (approx reasonably valid)

-  $\frac{d\delta}{dx} \ll 1$

-  $\frac{\partial \rho}{\partial y}$  small

①



t.e stall

$\frac{d\delta}{dx} \sim 0.1$

OK.

②



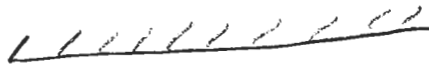
total or  
l.e stall

$\sim 1$

X

Large scale unsteadiness

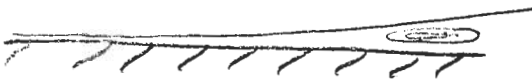
③



diffuser sep.

$\sim 0.1$

OK.



④



$\sim 1.0$

X

Large scale unsteadiness.

$\Rightarrow$  leads to IBLT lectures.

